#### Intercomparison Study of

Inductively Coupled Plasma Mass Spectrometry, Thermal Ionization Mass Spectrometry, and Fission Track Analysis

of µBq Quantities of <sup>239</sup>Pu in Synthetic Urine

#### **REPORT**

for

Department of Energy
Office of International Health Programs (EH-63)

Intercomparison Study of Inductively Coupled Plasma Mass Spectrometry, Thermal Ionization Mass Spectrometry and Fission Track Analysis of µBq Quantities of <sup>239</sup>Pu in Synthetic Urine

Kenneth G.W. Inn
National Institute of Standards and Technology
Ionizing Radiation Division
Gaithersburg, MD 20899

August 17, 1997



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### INTRODUCTION, APPROACH and TECHNICAL ISSUES

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#### Introduction

The Department of Energy, Office of International Health Programs (EH-63), is in the process of assisting Marshall Islanders to resettle their islands after five decades. The DOE and the resettled residents require assurances that the radiation dose to residents will not exceed recognized international standards or recommendations. One of the remaining radionuclides that could contribute to internal radiation dose from inhalation and ingestion intake pathways is <sup>239</sup>Pu. Since biological samples can be collected to quantitate the body content of radioactive materials or the damage created by exposure to ionizing radiation, the measurement of these parameters by instruments or analytical techniques must be accurately known. The uptake of <sup>239</sup>Pu is estimated from the excretion of <sup>239</sup>Pu in the urine of an individual. The analytical technique must have sufficient sensitivity to quantify <sup>239</sup>Pu at or below a level of 20 µBg/kg.

Until recently, Fission Track Analyses (FTA) of Marshall Islander urine has been the most sensitive measurement technique. Although FTA is very sensitive, it is also expensive and requires long turnaround times. Thermal Ionization Mass Spectrometry (TIMS) has had the potential sensitivity to equal that of FTA and could also provide isotopic information, but has never seriously been used for routine radiobioassay work because of the necessary laborious chemical purifications and rare expertise to knowledgeably operate the instrument. An emerging technology, Inductively Coupled Plasma Mass Spectrometry (ICP-MS), offers great potential as a rapid alternative ultrasensitive measurement method that is easy to operate and only requires a minimum amount of sample preparation. The attraction of faster, less expensive analyses of very low levels of plutonium in urine at comparable sensitivity motivated the Department of Energy to assess the capabilities of all three of these measurement techniques through this study.

The goal of this phase of the project is to evaluate the state-of-the-art (accuracy and precision) for <sup>239</sup>Pu in synthetic urine measurements by inductively coupled plasma (Brookhaven National Laboratory, BNL, and Pacific Northwest National Laboratory, PNNL), thermal ionization mass spectrometry (Los Alamos National Laboratory, LANL) and fission track analysis (BNL) in the concentration range of 18-278 µBq/g for 200g samples of synthetic urine. The major portion of the preparation tasks was performed by the Yankee Atomic Environmental Laboratory (YAEL), in terms of establishing the stability of <sup>99m</sup>Tc tracer <sup>239</sup>Pu in the synthetic urine, executing the dilutions, confirmational measurements and distributing the samples to participating laboratories. NIST oversaw the development of the work plan, YAEL's preparation of the test materials, and evaluation of the resulting data.

#### **Approach**

o NIST and its subcontractor, YAEL, developed a dilution and measurement confirmation scheme for the production of five replicate <sup>239</sup>Pu in synthetic urine

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at blank, 18.5, 46.3, 148.4, and 277.7 nBq/g samples for the three participating laboratories.

- o NIST, with YAEL, diluted the <sup>239</sup>Pu test solutions.
- o NIST and YAEL prepared the <sup>239</sup>Pu spiked synthetic urine samples, confirmed the dilutions by isotope dilution alpha spectrometry and <sup>99m</sup>Tc tracer gamma-spectrometry, and distributed five replicate samples at each concentration blind to Brookhaven, Los Alamos and Pacific Northwest National Laboratories.
- o NIST confirmed the YAEL dilution measurements.
- The participating laboratories had two months to report their final measurement data (including negative values) to NIST along with their evaluation of the uncertainties in their measurements.
- o NIST evaluated the resulting data to determine the accuracy, precision, sensitivity and limitations of the analyses of <sup>239</sup>Pu in synthetic urine:
  - Individual Laboratory Results: (Normality Tests)
     Data Distribution (Test for Measurement control)
     Mean Value (Bias)
     Variance (Precision)
     Identify Potential Measurement Discrepancies
  - Measurement Discrepancies:

Discuss measurement methodologies with laboratories Discuss sources of discrepancies to identify outlying data Evaluate likelihood of outlying data

Compare Laboratory Performances:

Data Distribution (Normality Tests)
Mean Value (Bias)
Variance (Precision)

Resolve Method Dependent Discrepancies:

Mean Value (Bias) Variance (Precision)

Technology Evaluation:

Bias
Precision
Minimum Detection Amount.

#### **Technical Issues**

A number of technical issues were raised during the design of the intercomparison protocols. These included:

- o Stability of the plutonium in glass bottles;
- o Stability of the plutonium in the synthetic urine;
- O Contamination from plutonium in the reagents used to make the synthetic urine; and
- o Adequacy of the synthetic urine as a substitute for natural urine.

Previous experience within the *in vitro* radiobioassay community indicated no particular problems with these issues. However, the issues must be reassessed in this intercomparison because of the extremely low concentrations of plutonium. These issues are addressed using the intercomparison data.

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# TEST SAMPLE PREPARATION, DILUTION VERIFICATION, TEST SAMPLE UNCERTAINTIES and REPORTING FORMAT

#### **Test Sample Preparation and Distribution Protocols**

The following steps describe the methodology used for preparation of <sup>239</sup>Pu in synthetic urine performance evaluation (PE) samples.

- 1. The <sup>239</sup>Pu standard was provided by NIST as a Standard Reference Material (SRM 4330A). Five ~ 50 mg aliquots of the SRM underwent alpha spectrometric analysis (sample IDs: 4330A-2 thru 6). The analyses were traced with <sup>242</sup>Pu. Counting statistics of ≤2% (1σ cs≤2%) were achieved for each measurement.
- 2. A 300 g solution of 4N HNO<sub>3</sub> was spiked with ~ 200 µCi of <sup>99m</sup>Tc. Sufficient <sup>99m</sup>Tc was added to achieve ≤1% counting statistics in a 5 minute counting interval for the dilution described in step 5. Prior to spiking the 4N HNO<sub>3</sub>, the <sup>99m</sup>Tc concentration in the purchased source was checked via gamma spectrometry of an ~ 1 g aliquot (sample ID: TC-CK1).
- 3. The <sup>239</sup>Pu SRM was diluted by a factor of 707.306 using the nitric acid solution from step 2. The diluted solution was ~ 250 g and was contained in a 500 mL capacity plastic bottle. Sample ID is 4330A-1. The diluted <sup>239</sup>Pu concentration was 5.358E-02 Bq/g. Five ~ 10 g aliquots of this dilution were verified via alpha spectrometry traced with <sup>242</sup>Pu (1σ cs≤2%). The verification sample IDs are 4330A-1B thru 1F.
- 4. Five samples, from step 3, were prepared for baseline gamma spectrometric verification by diluting ~ 10 g each of the solution to the required level in the counting container (sample IDs: 4330A-1G thru 1K). The diluent was unspiked 4N HNO<sub>3</sub>. The total weight of sample in the counting container will be ~ 70 g with a solution height of 3.8 ± 0.1 cm. All samples prepared for gamma spectrometry were counted in this geometry which is known as the "WATT-1" geometry. A blank 4N HNO<sub>3</sub> sample was also counted.
- 5. The solution from step 3 was diluted by a factor of 1268.806 using 4N nitric acid. The diluted solution was 3 kg and was contained in a cubitainer. The diluted <sup>239</sup>Pu concentration was 4.2231E-05 Bq/g. Sample ID is 4330A-1A.
- 6. Step 5 dilution was verified via gamma spectrometry (1σ cs≤1%) of five ~70 g aliquots in the WATT-1 geometry (sample IDs: 4330A-1A-1 thru 5). This measurement was compared with the baseline measurement of step 4. One blank aliquot of the 4N HNO₃ diluent also underwent gamma spectrometry. Steps 1 through 6 were performed within a 24 hour period to ensure that significant decay of <sup>99m</sup>Tc had not occurred prior to gamma spectrometry. The counting sequence was from the most diluted to the least diluted solution.

- 7. <sup>99m</sup>Tc was added to the solution remaining from step 6 in sufficient quantity (~5 mCi) to achieve ≤1% counting statistics for all subsequent dilutions. The <sup>99m</sup>Tc concentration in the purchased source was checked via gamma spectrometry of an ~ 0.1 g aliquot (sample ID: TC-CK2). A baseline gamma spectrometry of the "new" <sup>99m</sup>Tc in this solution was performed on five ~ 10 g aliquots diluted with 4N HNO₃ for the WATT-1 geometry (sample IDs: 4330A-1A-6 thru 10). One blank 4N HNO₃ was also counted. This solution is called the stock solution. A new, gravimetric based, <sup>239</sup>Pu concentration was recalculated for the stock solution (4.2209E-5 Bq/g). Sample ID of stock solution is 4330A-1A-11.
- 8. The stock solution from step 7 was diluted by a factor of 911.784 using synthetic urine. This dilution was prepared in a 10 kg cubitainer. The total weight of the diluted solution was 5 kg. The diluted <sup>239</sup>Pu concentration was 4.629E-08 Bq/g. Sample ID is PUR-250.
- 9. Step 8 dilution was verified via gamma spectrometry (1σ cs≤1%) of five aliquots in the WATT-1 geometry (sample IDs: PUR250-A thru E). <sup>99m</sup>Tc, added in step 7, was quantified. One blank synthetic urine aliquot was also analyzed.
- 10. Twenty 200 g aliquots of the solution prepared in step 8 were packaged into 16 oz. glass bottles with an exterior plastic coating. Five bottles each were shipped to two of the three participating labs, whereas ten bottles were shipped to the third lab.
- 11. The stock solution from step 7 was diluted by a factor of 284.492 using synthetic urine. This dilution was prepared in a 10 kg cubitainer. The total diluted solution weight was 5 kg. The diluted <sup>239</sup>Pu concentration was 1.484E-07 Bq/g. Sample ID is PUR-800.
- 12. Step 11 dilution was verified via gamma spectrometry (1σ cs≤1%) of five aliquots in the WATT-1 geometry (sample IDs: PUR800-A thru E). The analyte quantified was <sup>99m</sup>Tc which was added in step 7. One blank synthetic urine aliquot was also analyzed.
- 13. Twenty 200 g aliquots of the solution prepared in step 11 were packaged into 16 oz. plastic bottles. Five bottles each were shipped to two of the three participating labs, whereas ten bottles were shipped to the third lab.
- 14. The stock solution from step 7 was diluted by a factor of 151.9716 using synthetic urine. This dilution was prepared in a 10 kg cubitainer. The total diluted solution weight was 5 kg. The diluted Pu-239 concentration was 2.777E-07 Bq/g. Sample ID is PUR-1500.
- 15. Step 14 dilution was verified via gamma spectrometry (1σ cs≤1%) of five aliquots

- in the WATT-1 geometry (sample IDs: PUR1500-A thru E). The analyte quantified was <sup>99m</sup>Tc which was added in step 7. One blank synthetic urine aliquot was also analyzed.
- 16. Twenty 200 g aliquots of the solution prepared in step 14 were packaged into 16 oz. glass bottles. Five bottles each were shipped to two of the three participating labs, whereas ten bottles were shipped to the third lab.
- 17. The solution from step 14 was diluted by a factor of 15.004 using synthetic urine. This dilution was prepared in a 10 kg cubitainer. The total diluted solution weight was 5 kg. The diluted Pu-239 concentration was 1.851E-08 Bq/g. Sample ID is PUR-100.
- 18. Step 17 dilution was verified via gamma spectrometry (1σ cs≤1%) of five aliquots in the WATT-1 geometry (sample IDs: PUR100-A thru E). The analyte quantified was <sup>99m</sup>Tc which was added in step 7. One blank aliquot was also analyzed. Steps 7 through 18 were performed within a 24 hour period to ensure that significant decay of <sup>99m</sup>Tc had not occurred prior to gamma spectrometry. The counting sequence was from the most diluted to the least diluted PE sample.
- 19. Twenty 200 g aliquots of the solution prepared in step 17 were packaged into 16 oz. glass bottles. Five bottles each were shipped to two of the three participating labs, whereas ten bottles were shipped to third lab.
- 20. Twenty 200 g aliquots of the blank synthetic urine were also packaged into 16 oz. glass bottles. Five bottles each were shipped to two of the three participating labs, whereas ten bottles were shipped to the third lab.
- 21. The 200 g shipping aliquots of all the concentration levels were prepared 12 to 24 hours after the preparation of the PE materials.

#### **ATTACHMENT I**

#### REQUIREMENTS FOR CONFORMANCE

- 1. Two weights were recorded for each weighing. The precision of the two weights were within 0.5 percent. The mean of the two weights were used to calculate the gravimetric concentrations.
- 2. Counting statistics of 1% or better was achieved for all gamma spectrometric measurements. Counting statistics of 2% or better was achieved for all alpha spectrometric measurements.
- 3. All bottles packaged for shipping, including blanks, were assigned random ID numbers from 1 to 100. Higher concentration solutions, which were sent for fission track analysis, were labeled "high concentration."
- 4. 30 kg of synthetic urine was prepared in batches of 2 kg each. The batches were combined in a carboy and equilibrated for 24 hours. The synthetic urine was filtered through a 0.45µ filter (Gelman HT 450).
- 5. All glass bottles, used for shipping, were soaked for 72 h each in 0.1M disodium EDTA, 2M HNO<sub>3</sub> and 2M HCl. The bottles were rinsed with high purity deionized water and air dried.
- 6. All prepared solutions were shaken for at least 15 minutes before removing any aliquots.
- 7. All spikes, except the spike in step 16 were dispensed into the diluents via pycnometers. A 500-g poly bottle was used to deliver the 333.3 g spike in step 16.
- 8. The Mettler AE 163 analytical balance was used to determine the weights of the added spikes with the exception of the spike in step 16. The Mettler PM16-N balance was used to determine the weight of the spike dispensed in step 16. For the dilutions described in steps 10 and 13, multiple dispensations of the spikes were required due to the overall weight limit of 26 g on the AE 163 balance.
- 9. NIST prepared the certificates of content for the PE samples. The attached flowchart illustrates of the protocol described above.

#### ATTACHMENT II

#### **EQUIPMENT AND SUPPLIES**

- 1. GM survey meter
- 2. Log book, calculator, ruler, markers & pens
- 3. Gloves (L, M & S), safety glasses and lab coats
- 4. Absorbent paper, paper towels and kimwipes
- Radwaste bin
- 6. Non contaminated waste bin
- 7. Decon spray cans (hand and surface)
- 8. File for scoring ampoule
- 9. Plastic protectors for ampoule tip
- 10. Fifty pycnometers with elongated tips.
- 11. 500 mL and 1 gal. plastic bottles
- 12. Four 10L (2.5 gal) cubitainers and boxes
- 13. 50 kg carboy
- 14. 50 4 oz. plastic jars (counting containers for <sup>99m</sup>Tc) and plastic bags
- 15. Labels (w/ radioactive symbol) for <sup>99m</sup>Tc counting containers
- 16. Fifty gamma spec. measurement request forms (YELF 1101.1)
- 17. Duct, packing & electrical tapes
- 18. 25 HazMat multi pack shippers containing a 100 16 oz. glass bottles with exterior plastic coating.
- 19. 100 labels for shipping bottles
- 20. 25 FedEx Dangerous Goods Airbills, address labels and "Corrosive" labels
- 21. Reverse electrode germanium detector (40% relative efficiency)
- 22. Octet PC Alpha Spectrometer
- 23. Mettler AE 163 analytical balance with 5 digit precision and GA42 printer.
- 24. Mettler PM16-N top loader balance with 1 digit precision.

#### REAGENTS

- 1. High purity deionized water
- 2. 4M nitric acid 4 kg
- 0.1M Disodium EDTA
- 4. 2M nitric acid
- 5. 2M hydrochloric acid
- 6. Synthetic Urine 30 kg (see attached recipe)
- Pu-239 SRM
- 8. Tc-99m
- 9. Standardized Pu-242

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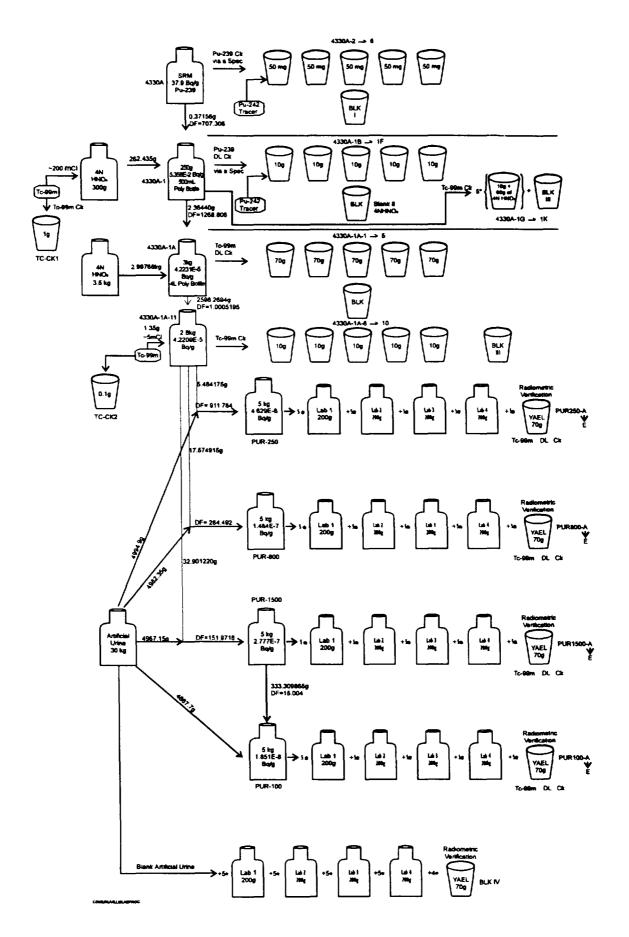
#### **RECIPE FOR SYNTHETIC URINE**

Component	g/kg
Urea	16.00
NaCl	2.32
KCI	3.43
Creatinine	1.10
Na₂SO₄ (anhydrous)	4.31
Hippuric Acid	0.63
NH₄CI	1.06
Citric Acid	0.54
MgSO₄ (anhydrous)	0.46
NaH₂PO₄ ● H₂O	2.73
CaCl₂ ● 2H₂O	0.63
Oxalic Acid	0.02
Lactic Acid	0.094
Glucose	0.48
Na₂SiO₃ ● 9H₂O	0.071
Pepsin	0.029
Conc. Nitric Acid	50.00
Yellow Food Color (optional)	0.06

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## Attachment III SAMPLE PREPARATION DESIGN

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## Attachment IV SRM 4330A Certificate

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## National Institute of Standards & Technology Certificate

#### Standard Reference Material 4330A Plutonium-239 Radioactivity Standard

This Standard Reference Material (SRM) consists of radioactive plutonium-239 nitrate and nitric acid dissolved in 5 mL of distilled water. The solution is contained in a flame-sealed NIST borosilicate-glass ampoule. The SRM is intended for the calibration of alpha-particle counting instruments and for the monitoring of radiochemical procedures.

#### Radiological Hazard

The SRM ampoule contains plutonium-239 with a total activity of approximately 210 Bq. Plutonium-239 decays by alpha-particle emission. None of the alpha particles escape from the SRM ampoule. During the decay process X-rays and gamma rays with energies from 10 keV to 1 MeV are also emitted. Most of these photons escape from the SRM ampoule but their intensities are so small that they do not represent a radiation hazard. Approximate unshielded dose rates at several distances (as of the reference time) are given in note [a]\*. The SRM should be used only by persons qualified to handle radioactive material.

#### Chemical Hazard

The SRM ampoule contains nitric acid (HNO<sub>3</sub>) with a concentration of 3 moles per liter of water. The solution is corrosive and represents a health hazard if it comes in contact with eyes or skin. If the ampoule is to be opened to transfer the solution, the recommended procedure is given on page 2. The ampoule should be opened only by persons qualified to handle both radioactive material and strong acid solution.

#### Storage and Handling

The SRM should be stored and used at a temperature between 5 and 65 °C. The solution in an unopened ampoule should remain stable and homogeneous until at least December 2005.

The ampoule (or any subsequent container) should always be clearly marked as containing radioactive material. If the ampoule is transported it should be packed, marked, labeled, and shipped in accordance with the applicable national, international, and carrier regulations. The solution in the ampoule is a dangerous good (hazardous material) both because of the radioactivity and because of the strong acid.

#### Preparation

This Standard Reference Material was prepared in the Physics Laboratory, Ionizing Radiation Division, Radioactivity Group, J.M.R. Hutchinson, Group Leader. The overall technical direction and physical measurements leading to certification were provided by L.L. Lucas of the Radioactivity Group.

The support aspects involved in the preparation, certification, and issuance of this SRM were coordinated through the Standard Reference Materials Program by N.M. Trahey.

Gaithersburg, Maryland 20899 January 1996 Thomas E. Gills, Chief Standard Reference Materials Program

\*Notes and references are on pages 5 and 6.

#### Recommended Procedure for Opening the SRM Ampoule

- 1) If the SRM solution is to be diluted, it is recommended that the diluting solution have a composition comparable to that of the SRM solution.
- 2) Wear eye protection, gloves, and protective clothing and work over a tray with absorbent paper in it. Work in a fume hood. In addition to the radioactive material, the solution contains strong acid and is corrosive.
- 3) Shake the ampoule to wet all of the inside surface of the ampoule. Return the ampoule to the upright position.
- 4) Check that all of the liquid has drained out of the neck of the ampoule. If necessary, gently tap the neck to speed the process.
- 5) Holding the ampoule upright, score the narrowest part of the neck with a scribe or diamond pencil.
- 6) Lightly wet the scored line. This reduces the crack propagation velocity and makes for a cleaner break.
- 7) Hold the ampoule upright with a paper towel, a wiper, or a support jig. Position the scored line away from you. Using a paper towel or wiper to avoid contamination, snap off the top of the ampoule by pressing the narrowest part of the neck away from you while pulling the tip of the ampoule towards you.
- 8) Transfer the solution from the ampoule using a pycnometer or a pipet with dispenser handle. NEVER PIPETTE BY MOUTH.
- 9) Seal any unused SRM solution in a flame-sealed glass ampoule, if possible, to minimize the evaporation loss.

See also reference [4]\*.

\*Notes and references are on pages 5 and 6.  $\frac{8}{15}$ 

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#### PROPERTIES OF SRM 4330A (Certified values are shown in bold type)

Source identification number	NIST SRM 4330A			
Physical Properties:				
Source description	Liquid in flame-seale	ed NIST borosilicate-g	lass ampoule	
Ampoule specifications	Body outside diamet Wall Thickness Barium content Lead-oxide content Other heavy element	(0.60 ± 0.1 Less than Less than	04) mm 2.5% 0.02%	
Solution density	$(1.0895 \pm 0.002) \text{ g} \cdot \text{r}$	nL <sup>-1</sup> at 24.9 °C [b]*		
Solution mass	Approximately 5.5 g			
Chemical Properties:				
Solution composition	Chemical Formula	Concentration (mol·L <sup>-1</sup> )	Mass Fraction (g•g <sup>-1</sup> )	
	H <sub>2</sub> O HNO <sub>3</sub> HCl <sup>239</sup> Pu+6	51 2.8 0.02 8 × 10 <sup>-8</sup>	0.84 0.16 0.0007 2 × 10 <sup>-8</sup>	
Radiological Properties:				
Radionuciide	Plutonium-239			
Reference time	1200 EST, 4 Decemb	per 1995		
Massic activity of the solution [c]	37.90 Bq·g <sup>-1</sup>		_	
Relative expanded uncertainty $(k=2)$	0.72% [d] [e]			
Alpha-particle-emitting impurities	None detected [f]			
Photon-emitting impurities	None detected [g]			
Half lives used in the decay corrections	Plutonium-239: (24	119 ± 26) a [h]		
Calibration method		ed-solid-angle counter a liquid-scintillation c		

<sup>\*</sup>Notes and references are on pages 5 and 6.

\*Notes and references are on pages 5 and 6.

	Method To Evaluate n(r.)	Relative Uncertainty	Relative Sensitivity	Relative Uncertainty
Input Quantity $x_t$ , the source of uncertainty	the standard uncertainty of $x_i$	Of Input Quantity,	Factor,	Of Output Quantity,
(and individual uncertainty components where appropriate)	(A) denotes evaluation by statistical methods (B) denotes evaluation by other methods	$u(x_i)/x_i,$ (%) [i]	(x <sub>i</sub> /y) [j]	$u_1(y)/y,$ $(\%)$ [K]
Massic alpha-particle emission rate, corrected for background and decay	Standard deviation of the mean for 10 sets of "0.1 $\pi$ " $\alpha$ measurements and 15 sets of $4\pi\alpha$ liquid-scintillation measurements (A)	0.05	1.0	0.05
Decay correction for plutonium-239	Standard uncertainty of the half life (A)	0.11 [m]	0.0005 [n]	0.00005
Decay-scheme data	Standard uncertainty of the probability of decay by alpha-particle emission (A)	0.001	0.1	0.001
Extrapolation of alpha-particle-count-rate-versus- energy to zero energy	Estimated (B)	0.25	1.0	0.25
Gravimetric measurements	Estimated (B)	0.10	0.1	0.10
Live-time [p]	Estimated (B)	0.10	1.0	0.10
Alpha-particle detection efficiency of scintillators	Estimated (B)	0.10	0.1	0.10
Geometry of "0.1n" a counter	Estimated (B)	0.25	0.4	0.10
Alpha-particle-emitting impurities	Limit of detection (B) [q]	100.	0.001	0.10
Photon-emitting impurities	Limit of detection (B) [q]	100.	0.001	0.10
Relative Combined Standard Uncertainty of the Ou	Output Quantity, $u_c(y)/y$ , (%)			0.36
Coverage Factor, k				x 2
Relative Expanded Uncertainty of the Output Quantity, U/y, (%)	ntity, <i>Uly</i> , (%)			0.72

#### NOTES

- [a] The Sievert is the SI unit for dose equivalent. See reference [1]. One  $\mu$ Sv is equal to 0.1 mrem. Distance from Ampoule (cm): 1 30 100
  Approximate Dose Rate ( $\mu$ Sv/h): <0.1 -
- [b] The stated uncertainty is two times the standard uncertainty.
- [c] Massic activity is the preferred name for the quantity activity per unit mass. See reference [1].
- [d] The reported value, y, of massic activity (activity per unit mass) at the reference time was not measured directly but was derived from measurements and calculations of other quantities. This can be expressed as  $y = f(x_1, x_2, x_3, \dots x_n)$ , where f is a mathematical function derived from the assumed model of the measurement process.

The value,  $x_i$ , used for each input quantity i has a standard uncertainty,  $u(x_i)$ , that generates a corresponding uncertainty in v,  $u_i(v) = |\partial y/\partial x_i| \cdot u(x_i)$ , called a component of combined standard uncertainty of v.

The combined standard uncertainty of y,  $u_c(y)$ , is the positive square root of the sum of the squares of the components of combined standard uncertainty.

The combined standard uncertainty is multiplied by a coverage factor of k = 2 to obtain U, the expanded uncertainty of v.

Since it can be assumed that the possible estimated values of the massic activity are approximately normally distributed with approximate standard deviation  $u_c(y)$ , the unknown value of the massic activity is believed to lie in the interval  $y \pm U$  with a level of confidence of approximately 95 percent.

For further information on the expression of uncertainties, see references [2] and [3].

- [e] The value of each standard uncertainty component, and hence the value of the expanded uncertainty itself, is a best estimate based upon all available information, but is only approximately known. That is to say, the "uncertainty of the uncertainty is large and not well known. This is true for uncertainties evaluated by statistical methods (e.g., the relative standard deviation of the standard deviation of the mean for the massic count rate is approximately 50%) and for uncertainties evaluated by other methods (which could easily be over estimated or under estimated by substantial amounts). The unknown value of the expanded uncertainty is believed to lie in the interval U/2 to 2U (i.e., within a factor of 2 of the estimated value).
- [f] Estimated limits of detection for alpha-particle-emitting impurities are:  $0.04 \quad \alpha \cdot s^{-1} \cdot g^{-1}$  for energies less than 4.9 MeV and  $0.001 \quad \alpha \cdot s^{-1} \cdot g^{-1}$  for energies greater than 5.2 MeV.

From mass-spectrometric measurements performed by the supplier, the massic activities of other detected radionuclides (in Bq·g<sup>-1</sup> at the reference time) are:  $^{240}$ Pu: 0.002;  $^{241}$ Pu:  $\approx 0.02$ ;  $^{242}$ Pu:  $\approx 0.000003$ ;  $^{241}$ Am:  $\approx 0.0009$ From the photon measurements below, we have  $^{241}$ Am:  $\leq 0.0006$ 

[g] Estimated limits of detection for photon-emitting impurities are:

0.000200 γ·s<sup>-1</sup>·g<sup>-1</sup> for energies between 42.5 and 90 keV,

0.000080 γ·s<sup>-1</sup>·g<sup>-1</sup> for energies between 102 and 125 keV,

0.000030 γ·s<sup>-1</sup>·g<sup>-1</sup> for energies between 133 and 1456 keV, and

0.000008 γ·s<sup>-1</sup>·g<sup>-1</sup> for energies between 1465 and 3500 keV,

provided that the photons are separated in energy by 4 keV or more from photons emitted in the decay of plutonium-239.

21/15%

- [h] The stated uncertainty is the standard uncertainty. See reference [5].
- [i] Relative standard uncertainty of the input quantity  $x_i$ .
- The relative change in the output quantity y divided by the relative change in the input quantity  $x_i$ . If  $|\partial y/\partial x_i| \cdot (x_i/y) = 1.0$ , then a 1% change in  $x_i$  results in a 1% change in y. If  $|\partial y/\partial x_i| \cdot (x_i/y) = 0.05$ , then a 1% change in  $x_i$  results in a 0.05% change in y.
- [k] Relative component of combined standard uncertainty of output quantity y, rounded to two significant figures or less. The relative component of combined standard uncertainty of y is given by  $u_i(y)/y = |\partial y/\partial x_i| \cdot u(x_i)/y = |\partial y/\partial x_i| \cdot (x_i/y) \cdot u(x_i)/x_i$ . The numerical values of  $u(x_i)/x_i$ ,  $|\partial y/\partial x_i| \cdot (x_i/y)$ , and  $u_i(y)/y$ , all dimensionless quantities, are listed in columns 3, 4, and 5, respectively. Thus, the value in column 5 is equal to the value in column 4 multiplied by the value in column 3. The input quantities are independent, or very nearly so. Hence the covariances are zero or negligible.
- [m] The relative standard uncertainty of  $\lambda \cdot t$  is determined by the relative standard uncertainty of  $\lambda$  (i.e., of the half life). The relative standard uncertainty of t is negligible.
- $[n] \qquad |\partial y/\partial x_i| \cdot (x_i/y) = |\lambda \cdot t|$
- [p] The live time is determined by counting the pulses from a gated oscillator.
- [q] The standard uncertainty for each undetected impurity that might reasonably be expected to be present is estimated to be equal to the estimated limit of detection for that impurity, i.e.  $u(x_i)/x_i = 100\%$ .  $|\partial y/\partial x_i| \cdot (x_i/y) = \{(\text{response per Bq of impurity})/(\text{response per Bq of Pu-239})\} \cdot (\{\text{Bq of impurity}})/(\{\text{Bq of Pu-239}\})\}$ . Thus  $u_i(y)/y$  is the relative change in y if the impurity were present with a massic activity equal to the estimated limit of detection.

#### REFERENCES

- [1] International Organization for Standardization (ISO), ISO Standards Handbook Quantities and Units, 1993. Available from the American National Standards Institute, 11 West 42nd Street, New York, NY 10036, U.S.A. 1-212-642-4900.
- [2] International Organization for Standardization (ISO), Guide to the Expression of Uncertainty in Measurement, 1993. Available from the American National Standards Institute, 11 West 42nd Street, New York, NY 10036, U.S.A. 1-212-642-4900. (Listed under ISO miscellaneous publications as "ISO Guide to the Expression 1993".)
- [3] B. N. Taylor and C. E. Kuyatt, Guidelines for Evaluating and Expressing the Uncertainty of NIST Measurement Results, NIST Technical Note 1297, 1993. Available from the Superintendent of Documents, U.S. Government Printing Office, Washington, DC 20407, U.S.A.
- [4] National Council on Radiation Protection and Measurements Report No. 58, A Handbook of Radioactivity Measurements Procedures, Second Edition, 1985. Available from the National Council on Radiation Protection and Measurements, 7910 Woodmont Avenue, Bethesda, MD 20814 U.S.A.
- [5] Evaluated Nuclear Structure Data File (ENSDF), December 1995.

# Dilution Verification

measured and gravimetrically determined dilution factors and the associated 1 sigma total propagated uncertainties. The reference and diluted materials with a HPGe detector. Table 1 summarizes the results of the verification measurements fourth column indicates the acceptance limit for the t test determination of any statistically significant difference between laboratory practice to verify the dilutions with measurements. It is particularly imperative to confirm the dilutions for this exercise because these are the first certified test materials of plutonium in the nBq/g range. Known quantities of semTc the measured and gravimetric dilution factors. As a whole, the measured dilution factors are not statistically different for the dilutions listed in the first column. The second and third columns indicates the percent difference between were added to the plutonium reference materials, and the subsequent dilutions were confirmed by measuring the Although dilutions of the sequential solutions could be calculated from the gravimetric determinations, it is good from the gravimetric dilution factors at the  $\alpha$  = 0.5 level.

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Dilution	Number of Replicate Sources	Percent Difference between Measured and Gravimetric Dilution Factors	Total Propagated 1 Sigma (%)	t <sub>0.975</sub> Test (%)
SRM 4330A to 4330A-1	5	-3.11	2.62	± 3.26
4330A-1 to 4330A-1A	5	-2.58	3.21	+ 3.98
4330A-1A-11 to PUR1500	5	-2.81	2.57	+ 3.19
PUR1500 TO PUR100	5	-1.87	2.58	± 3.21
4330A-1A-11 to PUR250	2	-3.76	2.60	± 3.23
4330A-1A-11 to PUR800	5	-3.03	2.50	+3.11

# Test Sample Uncertainties

Table 2 summarizes the test sample uncertainties. As a result of acceptable measurement verification of the gravimetric reference materials is from the gravimetric dilutions. These uncertainties were propagated as the root-sum-of-squares (Guidelines for Evaluating and Expressing the Uncertainty of NIST Measurement Results, B.N. Taylor and C.E. Kuyatt, NIST Technical Note 1297, NIST, Gaithersburg, MD, 1994) and reported as the relative expanded uncertainty for K = 2. dilution factors, the only additional uncertainty component that was propagated with the total relative uncertainty of the

Table 2

lable 2			ſ	
	Uncertainty Components	mponents		
Sample	Reference Material Total Uncertainty	Gravimetric	Sample Total Relative Uncertainty	Relative Expanded Uncertainty
Identification Number	1 s <sub>m</sub> , percent	1 s, percent	1 s <sub>m</sub> , percent	2s <sub>m</sub> , percent
SRM 4330A	0.36	•	0.36	0.7
4330A-1	0.36	0.14	0.4	0.8
4330A-1A	0.39	0.14	0.4	0.8
4330A-1A-11	0.41	0.14	0.4	6.0
PUR1500	0.44	0.14	0.5	1.0
PUR100	0.46	0.14	0.5	1.0
PUR250	0.44	0.14	0.5	1.0
PUR800	0.44	0.14	0.5	1.0

Fn:kinn/yael/puurine.pap/September 11, 1997

#### **Reporting Format**

The following reporting format was provided to the participating laboratories to organize the relevant information on their measurement protocols, results and the associated uncertainties.

### Results of Measurement <sup>239</sup>Pu in Synthetic Urine

1. Please use this data reporting form for the submission of analytical results. Twenty-five samples of <sup>239</sup>Pu spiked unstable synthetic urine (< 74000 nBq/sample) have been provided for this study. Because the long-term stability of the plutonium in the synthetic urine has not been determined, please analyze the total content of each bottle of sample (i.e., use the total content of a bottle for a single measurement), and report both the total activity and massic activity for each measurement result. Since the long-term stability of the samples has not been determined, it is strongly advised that each sample bottle is rinsed with > 3 M nitric acid, and the rinse solution be analyzed with the sample. The reference date and time for your reported results is:

#### 12:00 noon EST, February 26, 1997

2. Report <sup>239</sup>Pu measurements in Bq<sup>-</sup>g<sup>-1</sup> of solution. Report total combined standard uncertainty as 1s (%).

Sample Number	Total Activity (Bq) in each Bottle	Massic Activity (Bq·g·¹)	Uncertainty (% 1s)
		- 10 M	

e valvadamin			
	7 7 7 10		
-11-2			
	combined standard ur	mponents (random and ncertainty. These may	
	ue to calibration factor ue to dilutions/source		%. %.
Uncertainty d	ue to impurity correction	ons =%.	, o.
	ue to tracer calibration	n =%. surements =%.	
	as to grafilled to filed		
Uncertainty d Others; pleas	ue to spectral interfere	ences =%.	

4.	Describe in detail how the TEST samples were used, (i.e., give a detailed chronological description of the handling of the samples from the time they were opened to the time of reporting of results). This should include a description of solution transfer methodologies, chemical yield tracer additions, chemical separation used, measurement source preparation, storage of samples, etc. Please attach a separate page if necessary.
	<del></del>
5.	Describe the type of measurement system used, including a general description of its operation. Also indicate the type of analysis software utilized for any calculations and/or corrections applied to raw measurement data if applicable.
	· · · · · · · · · · · · · · · · · · ·

necessary.		 	

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 <del></del>		
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8. The deadline for submitted results is May 16, 1997. Please address results and technical questions to:

Kenneth G.W. Inn NIST 245/C114 Gaithersburg, MD 20899 Phone: 301-975-5541 Fax: 301-869-7682

email: kenneth.inn@nist.gov

#### **III**.

## NATIONAL LABORATORIES' ANALYTICAL METHODS

Attachments V, VI, VII and VIII are the reports of the analytical methods used by the national laboratories, the
incusurement results and the associated directionings. Table 5 summarkes the major analytical steps used by each laboratory.

Table 3

PNNL	Calcium Phosphate coppt, HNO <sub>3</sub> /H <sub>2</sub> O <sub>2</sub> dissolution	244Pu	2 N HNO <sub>3</sub> TEVA-Spec micro column, 6 N HCI wash, DI elution
LANL	Calcium Phosphate coppt from H <sub>2</sub> O <sub>2</sub> solution, dissolve in 8 N HNO <sub>3</sub>	<sup>242</sup> Pu	AG1X4, 8 N HNO <sub>3</sub> wash, 0.36 N HCI - 0.01 M HF elute, electrodeposit from NaHSO <sub>4</sub> soln, strip w/HF & HNO <sub>3</sub> , AG MP-1, 8 N HNO <sub>3</sub> , AG MP-1, 8 N HNO <sub>3</sub> wash, 0.5 N HCI & HI : HCI (1:9 vol.), AG-MP-1, H <sub>2</sub> O <sub>2</sub> -HCI wash, HBr elution
BNL FTA	Calcium Rhodizonate (pH > 9.5), coppt with EtOH, H <sub>2</sub> O <sub>2</sub> /HNO <sub>3</sub> microwave digestion, heat to dryness	Batch Yield Determination	Fe <sup>++</sup> + NO <sub>3</sub> -, AG1X4, 8N HNO <sub>3</sub> & HCI wash, HI/HCI elution, heat to dry, 8 N HNO <sub>3</sub> , micro anion exchange
BNL ICP-MS	Calcium Rhodizonate (pH > 9.5), coppt with EtOH, H <sub>2</sub> O <sub>2</sub> /HNO <sub>3</sub> microwave digestion, heat to dryness	<sup>242</sup> Pu	Fe <sup>++</sup> + NO <sub>3</sub> -, AG1X4, 8N HNO <sub>3</sub> & HCI wash, HI/HCI elution, heat to dry, 8 N HNO <sub>3</sub>
	Sample Preparation	Yield Monitor	Chemical Separations

Fn:kinn/yael/puurine.pap/September 11, 1997

DNS = dihydrogen dinitro sulfato platinate (II)

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## Attachment V BNL ICP-MS Report

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Saton New York The North

74 5 6 5 A.M. 2007 HAX HAS 344 5810 FINAL KAPLAN@BNL.GOV

Department of Advanced Technology Building 703M

June 6, 1997

Dr. Kenneth G.W. Inn **NIST** 245/C114 Gaithersburg, MD 20899

Dear Ken:

Many thanks for calling us concerning the fission track analytical and ICPMS data we reported to you on May 22nd. In this regard, please note the following corrections which we discussed this morning concerning data from fission track analyses:

- 1. For sample PUR0297-53, please change the reported massic activity from 31.3 μBq/kgm to 31.1 μBq/kgm,
- 2. With reference to the first paragraph on page 2 of my letter, we incorrectly identified the two samples lost during processing. Instead of using your sample identification numbers, we reported our internal fission track numbers. Thus what we reported earlier as sample PUR0297-34 was in reality your sample PUR0297-33. In addition, reported sample PUR0297-21 was actually PUR0297-62.

Samples PUR0297-12,93 were found to have many fewer tracks than expected (i.e., since they were part of the 5 replicates labeled as containing more than 1 fCi). As we discussed during earlier phone conversations, our FTA calibration curve has a maximum of about 500 aCi since in the normal course of our studies we usually do not encounter samples with much greater activity. For each these samples we placed droplets from our small column in pairs at three locations on the quartz substrate (instead of placing all six drops at a single location). Despite this precaution we still found more than 500 tracks for the first pairs, many of which were overlapping. Hence our initial estimates are known to be lower than expected. These samples have been recounted and show no significant changes in track count. Overlapping is attributable to the manner in which samples evaporate on the substrate, and increases with the amount of Pu in the sample. Our best conclusion is that counts of samples PUR0297-12,93 were lower than

expected, and we attribute this to our inability to distinguish individual tracks when they overlap in large numbers.

As mentioned, samples PUR0297-41,50 were on the same quartz substrate which was discolored (brown) when returned from the reactor. All other slides in the batch appeared normal except one, which contained two blanks and a flux monitor, and was returned discolored and deformed. We were unable to determine whether the discoloration could be related to objects on the slide (some recorded as tracks), and decided to report our findings as acceptable. These samples will also be recounted.

We are perplexed by sample PUR0297-41 for another reason. As we mentioned in our conversation, the location of this sample on the quartz substrate may have originally been incorrectly indicated in our logs. We surmise that we correctly identified the sample by comparing the pattern of tracks actually found with a sketch of the evaporated sample in our data book. Under normal operating procedures we would have reanalyzed this sample before reporting a result.

Records for samples PUR0297-51,91 have been reviewed and all appears in order. Under our normal protocol to minimize chances of false positives, we would have reanalyzed sample PUR0297-51 before reporting a result.

Apropos the ICPMS data, Rich Pietrzak is sending you a revised letter today. To summarize his findings, sample PUR0297-46 had a uniquely low chemical yield when compared to the entire set. The consequence of this is that the MDL for this sample alone is estimated at 5 uBq. Records for sample PUR0297-36 have been reviewed and all appears in order. There were also two typographical errors in our original letter. On page 2, item 3.5, change 12% to 9%. On page 3, next to last line from bottom, should read 55.6 μBq.

Thanks again for your interest. We look forward to hearing from you concerning these results.

Very truly yours,

Anant Moorthy, Ph.D.

Richard Pietrzak

Edward Kaplan, Ph.D., Group Leader Radiological Sciences Division

anth. Mos

EK/mcb

### BROOKHAVEN NATIONAL LABORATORY ASSOCIATED UNIVERSITIES INC

F 0 80+5000 potent New York 14 13 - 300

TB1 610.344-FAX 5107344-5810 E-MAIL KAPLAN@BNL.GOV

Department of Alayan red Technology

Building 703M

June 6, 1997

Dr. Kenneth G.W. Inn **NIST** 245/C114 Gaithersburg, MD 20899

Dear Ken:

We are taking the liberty of reporting the results of the samples you recently sent in letter format, rather than using the forms. Please note that the following correspond only to the samples analyzed via the mass spectroscopy analytical process.

Sample ID	Pu-239 μ <u>B</u> q	Uncertainty μBq Lower (at 1 sigma)	Uncertainty μBq Upper <u>(at 1 sigma)</u>	Pu-239 μBq/kg
PUR0297-16	3.4	3.1	3.6	16
PUR0297-18	0.1	-0.2	0.3	0.3
PUR0297-26	9.0	8.7	9.2	40
PUR0297-29	7.7	7.5	7.9	38
PUR0297-32	8.5	8.2	8.7	39
PUR0297-35	54.9	54.6	55.1	257
PUR0297-36	9.6	9.4	9.9	43
PUR0297-44	28.4	28.1	28.6	136
PUR0297-46*	-3.8	-4.1	-3.6	-19
PUR0297-52	31.3	31.1	31.6	149
PUR0297-54	8.8	8.6	9.1	41.5
PUR0297-57	55.6	55.3	55.8	263
PUR0297-58	3.3	3.1	3.6	15
PUR0297-65	2.8	2.6	3.0	12
PUR0297-70	58.1	57.9	58.4	255
PUR0297-71	-0.8	-1.1	-0.6	-4.1
PUR0297-74	28.3	28.1	28.6	134
PUR0297-75	3.6	3.3	3.8	16
PUR0297-79	55.9	55.7	56.1	257
PUR0297-81	29.2	29.0	29.4	136
PUR0297-84	57.9	57.7	58.1	262
PUR0297-85	9.4	9.1	9.6	44
PUR0297-87	29.7	29.5	30.0	138
PUR0297-92	0.6	0.3	0.8	3
PUR0297-100	0.2	-0.1	0.4	0.7

<sup>\*</sup>Low chemical yield gives an estimated MDL of 5  $\mu$ Bq.

Dr. Kenneth G.W. Inn June 6, 1997 Page 2

Our detection limit is approximately 50 aCi or 2  $\mu$  Bq. Values below this limit as well as negative results are included in the table for the benefit of statistical evaluation.

The following correspond to the items on your reporting forms.

#### Item #3:

1) Pu standard certification uncertainty: Pu-239 5%

Pu-242 0.74%

2) Pu standard preparation error: 3% (includes dilution error)

4) Mass Spectroscopy counting error: 3%

5) Pu recovery error in the chemistry procedure: 9%

Two major areas:

1) Co-precipitation step: 5%

2) Anion exchange column separation: 7%

#### Item #4: Procedure

The tapes around the glass NIST sample bottle caps were removed and the individual weights were noted. The samples were transferred to plastic containers for the co-precipitation step. To each empty bottle, 5 ml of conc. HNO<sub>3</sub> was added and the acid was sloshed around. They were stored for later addition to the samples. Synthetic urine blanks (a total of seven blanks) and spikes (a total of 16 spikes from 100 aCi to 2000 aCi) of volume equal to those of NIST samples were also analyzed along with the samples. Nominally equal amounts by weight of a Pu-242 tracer solution were added to both samples and synthetic urine blanks and spikes, and were stirred and allowed to equilibrate.

The pH of each sample was verified to be less than 2 and rhodizonic acid was added to each sample (100 mg for each 100 ml of sample) and stirred for 15 minutes. Then pH was adjusted to greater than 9.5 to precipitate calcium rhodizonate that carries the plutonium. An equal volume of ethanol was added to coagulate the precipitate, and the sample was allowed to stand overnight or longer.

The clear supernatant was decanted as much as possible and the slurry at the bottom was centrifuged in a polypropylene (PP) conical disposable centrifuge tube. The precipitate was dried at  $<90^{\circ}$  C, then dissolved in nitric acid and transferred to Teflon microwave digestion vessels. The concentrated HNO<sub>3</sub> wash contained in the original NIST bottle was also added to the vessels and microwaved to wet acid digest the samples.  $H_2O_2$  and HNO<sub>3</sub> were added during digestion as part of the microwave digestion cycle. The NIST sample bottles were then allowed to dry and were weighed to determine the tare weight.

Dr. Kenneth G.W. Inn June 6, 1997 Page 3

The clear solution, free of organic compounds, was evaporated to near dryness at low heat and the residue redissolved in 8N HNO<sub>3</sub>. Ferrous Ammonium sulfate was added while being warmed and stirred followed by NaNO<sub>2</sub> addition. The solution was passed through a conditioned 6 ml of anion exchange (AG1X4) resin, washed with 120 mL of sub-boiled 8N HNO<sub>3</sub> followed by 90 mL of sub-boiled 6N HCl. Plutonium was eluted by 30 mL of sub-boiled 6N HCl-0.1N HI into a tapered-quartz thimble and evaporated to dryness at about 90 degree centigrade.

The next set of procedures were performed inside a class 100 hood. The solution was taken up in 8N HNO, and transferred to small conical Teflon vials and again evaporated to dryness at about 90°C. The residue of plutonium was taken up in  $100 \, \mu L$  of 4N HNO3 and filtered through 2  $\mu m$  polypropylene syringe filters into 1 mL conical storage vials.

#### Item #5:

The samples were aspirated into the mass spectrometer for analysis. A HP4500 ICP-MS was fitted with a micro-concentric nebulizer for sample delivery to the plasma torch. A torch shield was used to minimize the instrument background. The instrument was tuned for maximum sensitivity with a 10 ppb Thallium solution in 2% HNO3. The quadrupole gain was adjusted to center the peak maxima for Pu-239 and 242. An aggregate accumulation time of 108.5 sec was used for each analysis. This process consumed the entire sample.

```
<u>Item #6:</u> Example calculation made for sample PUR0297-57
```

```
ICP-MS Number: MS97-74
Sample ID: PUR0297-57
Sample Mass: 211.3 (gm)
Accumulation period: 108.533 sec

Pu-239 (fg) = [Pu-242 fg]*(C239-B239)/(C242-B242)

for sample PUR0297-57

C239 = 4624 counts at m/e 239
B239 = 315.7 average blank counts at m/e 239
C242 = 8349
B242 = 315.7
Pu-242 = 44.53 fg

Pu-239 = 44.53(4624-315.7)/(8349-315.7)

Pu-239 = 23.88 fg = (23.88 fg) (0.01592 fg/aCi) = 1500 aCi = 55.6 μBq
```

#### The concentration is:

```
[Pu-239] = Activity/sample weight
= 55.6 \muBq/0.2113 kg
= 263.0 \muBq/kg
```

Dr. Kenneth G.W. Inn June 6, 1997 Page 4

The performance curve of observed Pu-239 activity versus the known ratio of Pu-239 to Pu-242, obtained with the results of synthetic urine blanks and spikes, was used to obtain linear regression parameters to evaluate the uncertainty in the sample measurements.

Using this technique, we obtain activity in sample PUR0297-57 1500 +/- 14 aCi at the 1 sigma confidence level.

Expressing these in  $\mu$ Bq, we use the conversion factor = 0.037037  $\mu$ Bq/aCi to obtain 55.6  $\pm$  0.5  $\mu$ Bq. For massic activity, divide activities above by corresponding sample mass (211.3 gm in this case) to obtain 263  $\mu$ Bq/kgm.

With the delivery of the results for both fission track and mass spectroscopy analysis we would like to have the actual spike levels for each sample so that we can further evaluate the results. Moreover, these comparisons are necessary for the FY98 program planning, which we are now in the process of formulating and will be reported to DOE within the next several weeks. If there are any questions, please feel free to call either of us at (516) 344-5539 (R. Pietrzak) or (516) 344-2007 (E. Kaplan).

Sincerely yours,

Richard Pietrzak

Richard Pietrzak

Rochert Rochert

Edward Kaplan, Ph.D., Group Leader Radiological Sciences Division

EK/mcb encl.

Attachment VI

BNL FTA Report

#### BROOKHAVEN, NATIONAL LABORATURY

ASSOCIATED UNIVERSITIES INC

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TEL (516 344)

FAX (210.344-5810 FAMA: KAPLAN@BNL.GOV

Department of Advanced Technology

Building 703M

May 22, 1997

Dr. Kenneth G.W. Inn NIST 245/C114 Gaithersburg, MD 20899

Dear Ken:

We are taking the liberty of reporting the results of the samples you recently sent in letter format, rather than using the forms you provided. Please note that the following correspond only to the samples analyzed via the fission track analytical process.

Total Activity.

Lineartainty

	Total Activity	Uncertainty	
	in Each	(one sigma) <sup>1</sup>	Massic
Sample	Bottle	(Lower/Upper)	Activity
Number	(µBq)	(µBq)	(µBq/kgm)
PUR0297-01	*	*	*
PUR0297-04	2.5	2.2/2.8	11.1
PUR0297-06	0.7	0.4/1.0	3.3
PUR0297-08	1.7	1.4/2.0	7.8
PUR0297-12	27.1	26.8/27.5	123
PUR0297-15	*	*	*
PUR0297-20	23.2	22.9/23.6	100
PUR0297-31	11.4	11.1/11.7	52.5
PUR0297-40	10.0	9.6/10.3	44.9
PUR0297-41	18.2	17.8/18.5	77.6
PUR0297-42	57.0	56.5/57.5	275
PUR0297-50	2.6	2.3/2.9	12.3
PUR0297-51	9.1	8.8/9.4	42.4
PUR0297-53	6.9	6.6/7.2	31.7 1
PUR0297-59	6.1	5.8/6.4	27
PUR0297-60	3.1	2.8/3.4	14.3
PUR0297-63	2.9	2.5/3.2	12.5
PUR0297-73	48.9	48.5/49.4	237
PUR0297-80	34.1	33.7/34.5	161
PUR0297-83	*	*	*
PUR0297-91	3.2	2.8/3.5	14.1
PUR0297-93	21.6	21.3/22.0	104
PUR0297-96	*	*	*

<sup>&</sup>lt;sup>1</sup>See explanation for item 6.

Dr. Kenneth G.W. Inn May 22, 1997 Page 2

Items below our detection limit (3 sigma of blanks approximately 20-25 aCi, 0.7-0.9 uBq) are indicated with an asterisk. Two samples were lost during processing: sample PUR0297-034 was lost as it was being placed onto the substrate, and sample PUR0297-021 was contaminated with plutonium that was intended for use as a flux monitor. Please note that had we followed our standard protocol, where we process only part of the sample, we would have been able to reanalyze these two lost samples.

Based particularly on our Marshall Islands experience, and as we state in our publications, we are more concerned with false positives than with false negatives. We therefore use this same protocol to reanalyze samples over 10x our detection limit. Unfortunately this was not possible using your instructions. For the same reasons, we also usually report our results at the 99% confidence level, rather than 1 sigma, as you requested.

The following correspond to the items on your reporting forms.

#### Item #3:

- 1) Pu standard certification uncertainty: 5%
- 2) Pu standard preparation error: 3% (includes dilution error)
- 3) Thermal neutron flux error: 10% (includes uncertainty in Pu quantity in the flux)
- 4) Fission Track counting error: 3%
- 5) Pu recovery error in the chemistry procedure: 15%

(Three major areas:

1) Co-precipitation step: 5%
2) 1st column separation: 7%, and
3) micro-column separation: 12%)

#### Calibration curve:

The calibration curve reflects the sum-total of all the aforementioned errors. An additional uncertainty is the variation found in tracks for synthetic urine (i.e., fission tracks attributable to <sup>239</sup>Pu in the reagents and interfering fission tracks from <sup>235</sup>U that is also present in the reagents and the process). This uncertainty affects the estimation of <sup>239</sup>Pu concentration in samples to a varying degree, that is, it is higher for activity closer to the MDL than it is for activities at the higher end of the calibration region. For example, 70 aCi samples, at the 99% confidence level the error can be about 60%, and at 200 aCi levels, it can be about 30%.

#### Item #4:

The tapes around the glass NIST sample bottles were removed and the individual weights were noted. The samples were transferred to plastic containers for co-precipitation step. The empty bottles were weighed and noted. To each empty bottle, 5 ml of conc. HNO<sub>3</sub> was added and the acid was sloshed around. They were stored for later addition to the samples. Synthetic urine blanks (a total of seven blanks) and spikes (a total of 16 spikes from 100 aCi to 400 aCi) of equal volume to those of NIST samples were also analyzed along with the samples.

blank cometin = not constant why?

Dr. Kenneth G.W. Inn May 22, 1997 Page 3

The pH of each of the sample was adjusted to between 2 and 3 and rhodizonic acid was added to each sample (100 mg for each 100 ml sample) and stirred for 15 minutes. Then pH was adjusted to greater than 9.5 to precipitate calcium rhodizonate that carries plutonium. An equal volume of ethanol was added to coagulate the precipitate, and the sample was allowed to stand overnight or longer.

The clear supernatant was decanted as much as possible and the slurry at the bottom was centrifuged in a polypropylene (PP) conical disposable centrifuge tube. To each centrifuge tube conc. HNO<sub>3</sub> wash contained in the original NIST bottle was added and microwaved for wet acid digestion. H<sub>2</sub>O<sub>2</sub> and HNO<sub>3</sub> were added during digestion as part of microwave digestion program.

The clear solution, free of organic compounds, was evaporated to dryness at low heat and the residue re-dissolved in 8N HNO<sub>3</sub>. Ferrous ammonium sulfate was added while being warmed and stirred followed by NaNO<sub>3</sub> addition. The solution was passed through a conditioned 6 ml of anion exchange (AG1X4) resin, washed with 3 column volumes of sub-boiled 8N HNO<sub>3</sub> followed by 3 volumes of sub-boiled 6N HCl. Plutonium was eluted by 7 column volumes of sub-boiled 6N HCl-0.1N HI into a tapered-quartz thimble and evaporated to dryness at about 90 degree centigrade.

The next set of procedures were performed inside a class 100 hood. The solution is taken up in 8N HNO, and passed through a 12  $\mu$ l micro-column of an anion exchange resin to remove uranium and other ions. Plutonium was eluted in three drops which were collected on a cleaned Suprasil surface, dried under an infrared lamp, packaged under vacuum and irradiated using a thermal neutron fluence of 9E16 n/cm<sup>2</sup>.

After irradiation the slides were cleaned and etched in conc. HF for 105 seconds. The enlarged tracks were counted under a microscope.

#### Item #5:

During fission track counting, a slide was loaded onto a holder and placed on a stage under the magnifying lens of a microscope. As per the flow diagram of attached figures, each Suprasil slide was divided into three equal  $1 \text{cm}^2$  areas with each area representing a sample (Right, Center and Left). Each area of  $1 \text{ cm}^2$  was further divided into a 24 x 34 (816 frames) matrix to be examined under the microscope. A total magnification of 160 is used. A computer program controls the movement of the stage holding the slide automatically, from the beginning of a row of frames to the end when the stage drops to the next row by one frame and the scanning continues until all 816 frames are completed. During scanning the stage can be stopped for counting the tracks. An average of about 15 to 20 minutes is required for each sample.

Item #6: Example calculation is made for sample PUR0297-08

Fission Track Number: 97-004 Sample ID: PUR0297-08 Sample Mass: 216.5 (gm)

Tracks: 70

Calibration curve using blanks and spikes gives:

Tracks =  $b_0 + b_1 * (Activity [aCi])$ 

where:  $b_0 = 20.47$ 

 $b_1 = 1.08$ 

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> For an inverse regression, we obtain (see Eq. [1.7.5] from Draper, N.R. and H. Smith, Applied Regression Analysis, J. Wiley & Sons, 1981, pp 47-51).

$$\frac{X_U}{X_L} = \bar{X} + \frac{b_1(Y_0 - \bar{Y}) \pm ts\{[(Y_0 - \bar{Y})^2/S_{xx}] + (b_1^2/n) - (t^2s^2/nS_{xx})\}^{1/2}}{b_1^2 - (t^2s^2/S_{xx})}$$

where:

X = activity of a urine sample,

Y = tracks found for a urine sample,

s = variance about the calibration curve,

 $S_{xx}$  = sum of squares of residuals of activities in synthetic urine spikes,

t = Student's t-distribution with n-2 degrees of freedom at some specified confidence level,

n = number of synthetic urine blanks and spikes,

X<sub>bar</sub> = average activity of synthetic urine spikes used in calibration curve,

Y<sub>bar</sub> = average tracks of synthetic urine blanks and spikes used in calibration curve,

and where 1 + 1/n should be used instead of 1/n to reflect that an individual observation is being used (instead of a population mean).

Using this equation, we obtain activity in sample PUR0297-08 of  $46 \pm 9$  aCi at the 1 sigma confidence level.

Expressing these in uBq, we use the conversion factor= 0.037037 uBq/aCi to obtain  $1.7 \pm 0.3$  uBq. For massic activity, divide the activity by the sample mass (216.5 gm) to obtain 7.8 uBq/kgm.

As I mentioned in our recent phone conversation, and as confirmed with Neil Barss (DOE/EH-63), we expect to report results using ICPMS by May 30th.

Very truly yours,

Anant Moorthy, Ph.D.

Edward Kaplan, Ph.D., Group Leader

Radiological Sciences Division

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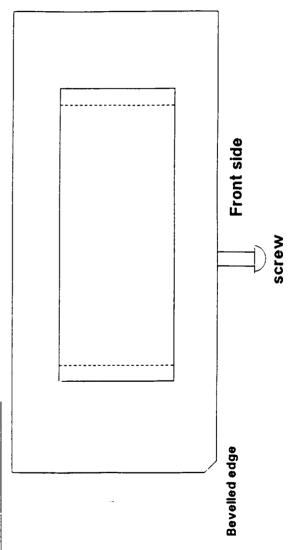
EK/jk encl.

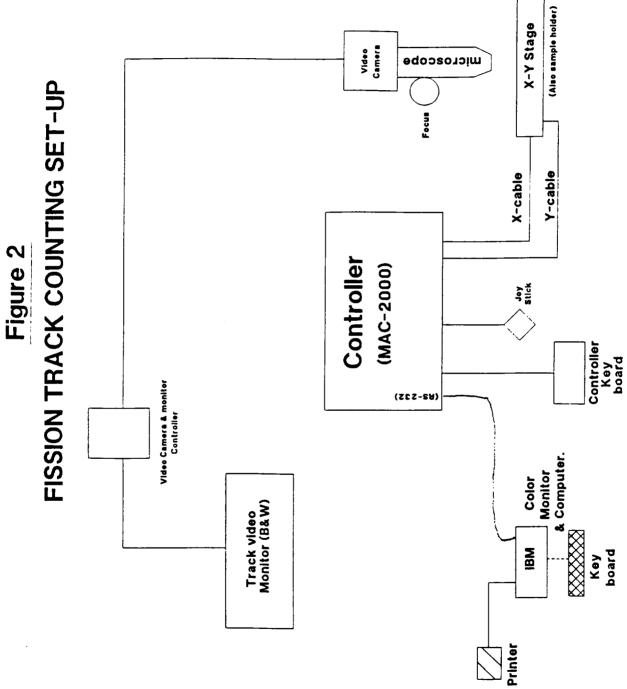
# Slide and slide holder Figure 1

(not to scale)

¶ mm €.₽1-(1eft) 38.1 mm X (0,0) (Front side) (center) (Right) 1) slide (quartz)

2) Slide Holder (aluminum)





## Attachment VII LANL TIMS Report

#### UNCLASSIFIED FACSIMILE

LOS ALAMOS NATIONAL LABORATORY ANALYTICAL QUALITY AND CHEMICAL INFORMATION MANAGEMENT (CST-3)

P.O. BOX 1663, MS K484 LOS ALAMOS, NM 87545 FAX NO: (505) 665-5982 CONFIRMATION NUMBER: (505) 665-7323

TOTAL PAGES ( DATE: 5 - \	NCLUDING COVER SHEET): 15 3-97
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TO:	FAX NO:
TO:	FAX NO:
	sults of Measurement  Du in Artificial Urine!
COMMENTS:	hard copy to follow in
	* mail.
	`A
OPERATOR:	Cardyn J. Macdonell

#### Results of Measurement of <sup>239/240</sup>Pu in Artifical Urine Los Alamos National Laboratory

Contact Person: Moses Attrep, Jr. (505) 667-0088

1. Please use this data reporting form for the submission of analytical results. Twenty-five samples of <sup>239/240</sup>Pu spiked unstable artifical urine (<10,000 aCi/sample) have been provided for this study. Please analyze the total content of each bottle of sample, and report the individual measurement results. The reference date and time for your reported results are:

#### 12:00 noon EST. February 26, 1997

2. Report measurement in Bq'g' of solution. Report total combined standard uncertainty as 1s (%).

Table I. I.	os Alamos	National:	Laboratory	Results	for	Plutonium	Samples.
-------------	-----------	-----------	------------	---------	-----	-----------	----------

MOWIC ID X	Sample Number	Total Activity (Bq) in Each Bottle	Massic Activity (Bq'g'-1)	Uncertainty (% 1s
PUR0897	(LANE)	III Daon Doute	(DQZ)	
্ড	00.35866	7.40 E-05	3.30E-07	8.2
09	00.35867	4.77 E-05	2.23 E-07	12.2
11	00.35868	2.78 E-05	1.28 E-07	17.6
13	00.35869	2.31 B-05	1.09 E-07	19.4
19	00.35870	3.62 E-05	1.76 E-07	17.1
21	00.35871	7.45 E-05*	3.44 E-07*	10.9
22	00.35872	2.23 E-05	1.01 E-07	22.5
25	00.35873	1.90 E-05	8.44 E-08	35.5
27	00.35874	5.44 B-05	2.54 E-07	8.7
37	00.35875	6.45 E-06	2.93 E-08	70.2
39	00.35876	1.55 B-05	7.12 E-08	32.9
45	00.35877	8.83 E-06	3.97 E-08	58.4
47	00.35878	1.76 E-05	7.94 E-08	28.5
48	00.35879	6.90 E-06	3.19 E-08	66.7
(e)	00.35880	2.34 B-06	1.08 E-08	184.3
lola	00.35881	7.83 E-06	3.59 E-08	59.5
68	00.35882	-1.78 E-06*	-8.84 E-09*	249.1
77	00.35883	2.83 E-05	1.45 E-07	31.6
78	00.35884	1.68 E-05*	8.26 E-08*	28.7
85	00.35885	6.99 E-06	3.13 E-08	78.2
86	00.35886	-2.31 E-06	-1.11 E-08	195.4
89	00.35887	1.28 E-05	5.90 E-08	37.2
90	00.35888	1.15 E-05	5.60 E-08	39.0
_ 95 L	00.35889	1.09 E-04*	4.92 E-07*	13.9
98	00.35890 *Upper limit	-1.49 E-06	-7.14 E-09	294.4

Opper limit

3. The ±1s "standard uncertainty" components (random and systematic) which comprise the combined standard uncertainty. These may include, but not limited to the following:

Uncertainty due to calibration factor/efficiency:
Uncertainty due to dilutions/source preparation:
Uncertainty due to impurity corrections:
Uncertainty due to tracer calibration:
Uncertainty due to gravimetric measurements:
Uncertainty due to spectral interferences:
Uncertainty due to spectral interferences:

-0.1%
Others, please describe.

The errors reported for these results are reflective of the uncertainties of the thermal ionization measurements. These uncertainties are larger than the uncertainties due to other measurements (weighing, etc.) stated above.

4. Describe in detail how the TEST samples were used, (i.e., give a detailed chronological description of the handling of the samples from the time they were opened to the time of reporting of results). This should include a description of solution transfer methodologies, chemical yield tracer additions, chemical separation used, measurement source preparation, storage of samples, etc. Please attach a separate page if necessary.

Note: The procedures and other information are included in the report and are not placed on separate pages.

The standard procedure for plutonium bioassay samples at Los Alamos National Laboratory was used for these samples. This included (a) preparation for alpha counting, (b) stripping off disc and preparation for TIMS, and (c) TIMS analysis and data reduction. This includes a calcium phosphate precipitation and a nitric acid column purification before electro deposition and counting. Following counting the plutonium is stripped from the discs and purified by two columns before TIMS preparation and instrumental analysis.

#### 1.0 Removing Sample from Bottles

- 1.1 The samples were logged into the sample management system and stored at ~4° C until they were delivered to TA-48 for processing. Upon arrival at TA-48, RC-45, our clean room facility, the samples were stored in a refrigerator at ~4° C until processing commenced.
- 1.2 Sets of 12 samples which included QA samples and process blanks were taken to the first laboratory for initial processing. The outer plastic cover was removed and the lids were unscrewed to allow the pressure in the bottles to come to our atmospheric pressure and the lids were rescrewed.
- 1.3 The samples were then weighed on a single pan balance ( $\pm$  0.3 g). From each sample 0.5 mL was removed for making a specific gravity measurement. The bottle was then reweighed. The contents of the bottle were then delivered

into a new, clean 400 mL beaker. The bottle was then rinsed three times with approximately 3 mL of 8 M HNO<sub>3</sub> and the contents added to the beaker. The bottle and cap was then rinsed with water and allowed to dry before being reweighed. The amount of sample was determined from the weighings.

#### 2.0 Radiochemical Purification Procedure

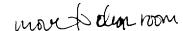
- 2.1. <u>Preparation of 500 g of Bio-Rad AG 1-X4, 100-200 mesh resin for the anion exchange of plutonium.</u>
- 2.1.1. To remove the fines, pour 500 g of resin into a 2-L beaker and add water to give a volume of approximately 1600 mL.
- 2.1.2. Stir the slurry on a magnetic stirrer for 20 min.
- 2.1.3. Slowly decant the water along with the fines when the bulk of the resin settled.
- 2.1.4. Repeat Steps 2.1.1 to 2.1.3 two using 8 M HNO<sub>3</sub> instead of water. A final rinse is made with water.
- 2.1.5. Store the resin slurry in the orginal bottle in water.
- 2.2. Chemical separation of plutonium in sample.

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- 2.2.1. Add 5 to 10 drops of 1-octanol to the sample if sample is foamy.
- 2.2.2. Add 1.0 mL of the <sup>242</sup>Pu tracer solution.
- 2.2.3. Add 200 μL of Ca(NO<sub>3</sub>)<sub>2</sub> solution.
- 2.2.4. Add 1 mL of concentrated H<sub>3</sub>PO<sub>4</sub>.
- 2.2.5. Add 10 mL of 30% H<sub>2</sub>O<sub>2</sub>.
- 2.2.6. Add 100 mL of conc NH4OH.
- 2.2.7. Cover the beakers with Parafilm™ and let samples precipitate overnight.
- 2.2.8. Remove the Parafilm™ and decant if the solution is clear.
- 2.2.9. Pour the remaining slurry into a 250-mL Teflon bottle. Screw cap on
- 2.2.10. Centrifuge for 5 min.

- 2.2.11. Remove cap and pour off supernatant solution.
- 2.2.12. Add an equal amount of conc HNO<sub>3</sub> to the precipitate slurry and cap loosely. Swirl to dissolve particles adhering to the surface of the bottle.
- 2.2.13. Add 75 mL of 8 M HNO<sub>3</sub> to the bottle. Heat on the hot plate that has a surface temperature of 120-150° C for 1.5 hours.
- 2.2.14. Cover samples and transfer to clean room.



- 2.3. Anion exchange separation.
- 2.3.1. Put a plug of glass wool into the bottom of the anion exchange column and fill the column with AG 1-X4, anion exchange resin to a height of 6-7 cm. Wash the column with H<sub>2</sub>0 until the resin column maintains a constant level.
- 2.3.2. Wash the column reservoir with 75 mL of 8 M HNO<sub>3</sub> and allow the solution to pass through the column. Discard the eluent.
- 2.3.3. Pour the sample into the column reservoir.
- 2.3.4. When all of the sample has been transferred to the column reservoir and has completely drained, rinse the bottle with 8 M HNO<sub>3</sub> and pour the washings into the column reservoir. Wash the bottle two additional times with 5-10 mL 8 M HNO<sub>3</sub>.
- 2.3.5. When the 8 M HNO<sub>3</sub> solution has drained, wash the walls of the reservoir with 8 M HNO<sub>3</sub>. Repeat this washing three additional times.
- 2.3.6. Fill the reservoir with 75 mL of 8 M HNO<sub>3</sub>, drain down to the top of the column.
- 2.3.7. Place a 100-mL beaker under the column after all the wash solution has flowed through the column.
- 2.3.8. Add 2 mL of 5% NaHSO<sub>4</sub> solution to the 100-mL beaker.
- 2.3.9. Add 25 mL of 0.36 M HCl-0.01 M HF eluting solution to the column.
- 2.3.10. Collect the effluent in the beaker containing the 5% NaHSO<sub>4</sub>. Evaporate the slurry to dryness on a hot plate with a surface temperature of 120-150°C for the first 30 min because the solution may splatter. After the sample has been dried, add 5 mL concentrated HNO<sub>3</sub> and 1 mL of 30% H<sub>2</sub>O<sub>2</sub>. Take to dryness on the hot plate. Repeat HNO<sub>3</sub>-H<sub>2</sub>O<sub>2</sub> treatment, if necessary.

- 2.3.11. Remove beaker from hot plate and allow to cool.
- 2.4. Electrodeposition.
- 2.4.1. Add 4 mL of the electrolyte solution (15% Na<sub>2</sub>SO<sub>4</sub>) to the beaker and allow to set for 20-30 minutes.
- 2.4.2. Engrave back of stainless steel disc with sample numbers.
- 2.4.3. Assemble the cell, placing the disk into the bottom depression of the cap, and screw together.
- 2.4.4. Fill the cell with water to test for leaks. Discard the water.
- 2.4.5. Add the sample solution to the cell.
- 2.4.6. Rinse the sample beaker with water and add the wash to the cell. Fill the cell with water to within 14 mm of the top of cell.
- 2.4.7. Place the cell in the electrodeposition rack so that the platinum wire electrode is inserted into the cell. The bottom of the platinum electrode is 12 mm from the stainless steel disc.
- 2.4.8. Attach the cathode lead to the cell cap.
- 2.4.9. Turn on the main switch of the electrodeposition unit. Set current to 0.5 amps.
- 2.4.10. Electroplate for 180 min.
- 2.4.11. Add 1 to 2 mL of 25% NaOH to the cell and after 60 seconds turn off the current.
- 2.4.12. Pour the solution out of the cell and disassemble the cell. Wash the stainless steel disc with  $H_20$ . Be sure not to touch the surface of the disc.
- 2.4.13. Dry the disk in the coin holder on the hot plate set on "low"; label coin holders with sample identification.
- 2.5. Samples are delivered to count room for a 70,000 sec alpha count.
  Following counting, the samples are returned to clean room for processing for thermal ionization mass spectrometry analysis.
- 2.6. Strip from Stainless Steel Discs and Final Anion Columns for Bioassay Samples.

- 2.6.1. Place the stainless steel disc on top of an inverted 50 mL Teflon beaker. Add 2 drops of conc HF and evaporate to dryness under a heat lamp. Add 2 drops of conc HNO<sub>3</sub> to the disc and evaporate to dryness.
- 2.6.2. Rinse the plutonium from the disc with conc HNO<sub>3</sub> into a 40 mL centrifuge tube. Evaporate the nitric acid solution containing the plutonium to dryness.
- 2.6.3. A Poly-Prep<sup>™</sup> chromatography column (Bio-Rad) is filled to the 1.8 mL level with AG MP-1, 50-100 mesh, anion exchange resin. The resin is conditioned with three 2 mL additions of 8 M HNO<sub>3</sub>.
- 2.6.4. The sample is taken up using 2 mL of 8 M HNO<sub>3</sub> and loaded onto the column. The sample tube is washed with two 1-mL additions of 8 M HNO<sub>3</sub> and the wash is added to the column allowing the solution to drain completely between each addition. Finally, the column is rinsed with three 2-mL additions of the 8 M HNO<sub>3</sub>.
- 2.6.5. A clean centrifuge tube is placed under the column and the plutonium is eluted by adding three 1.5-mL additions of 0.5 M HCl followed by three 2 mL additions of the HI-HCl reagent (1:9 ratio, by volume HI to HCl).
- 2.6.6. The sample is evaporated to dryness. One mL of conc HNO<sub>3</sub> is added and the sample is evaporated to dryness again. Finally 1 mL of conc HCl is added and the sample is taken to dryness.
- 2.6.7. A small anion exchange chromatography column is prepared by placing AG MP-1, 50-100 mesh resin in a disposable pipette tip that is 7-cm in length by 5-mm in diameter. Prewashed quartz wool plug is inserted in the pipette tip and resin is added to a depth of 2 cm.
- 2.6.8. The column is conditioned with two 1-mL additions of a H<sub>2</sub>O<sub>2</sub>-HCl reagent (2 drops of 30% H<sub>2</sub>O<sub>2</sub> to 10 mL conc HCl) that is freshly prepared.
- 2.6.9. The sample is dissolved with 1 mL of the H<sub>2</sub>O<sub>2</sub>-HCl solution and loaded onto the column. The sample tube is washed with two 1-mL additions of the H<sub>2</sub>O<sub>2</sub>-HCl solution and added to the column.
- 2.6.10. The column is rinsed with four 0.75-mL additions of 8 M HNO<sub>3</sub>. The solution is allowed to drain completely each time before adding the next rinse.
- 2.6.11. The plutonium is eluted from the column into clean 10 mL quartz test tubes using three 0.75-mL additions of conc HBr. Each addition is allowed to drain completely before adding the next.
- 2.6.12. The HBr is evaporated to dryness.

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- 2.6.13. Seven drops of conc HNO₃ and 7 drops of conc HClO₄ are added to each sample and heated at 180° C until dry in a heat block. The sample is cooled to room temperature and 10 drops of conc HCl are added. The sample is slowly evaporated in a heat block until dry.
- 2.6.14. The samples are submitted for mass spectrometric analysis.
- 2.7. Thermal Ionization Mass Spectrometric Filament Preparation.

The mounting of the previously purified plutonium sample is accomplished by electrodeposition of the plutonium with a small quantity of platinum. A larger quantity of platinum is then electrodeposited over the plutonium to provide a diffusion barrier which dissociates plutonium molecular species and provides high ionization efficiency.

- 2.7.1. The electrodeposition apparatus is assembled with parts that have been cleaned and stored in the clean room.
- 2.7.2. One hundred  $\mu$ L of 1.5 M NH<sub>4</sub>Cl (buffered to pH 2.8 with pure ammonia gas) and 10  $\mu$ L of 1.5 M HCl are added to the quart tube containing the chemically purified plutonium sample.
- 2.7.3. The solution is warmed with a heat lamp for 2 minutes and 5  $\mu$ L of DNS (dihydrogen dinitrosulfatoplatinate (II), 2  $\mu$ g/mL in 1.5 M HCl) is added.
- 2.7.4. The solution is transferred with a transfer pipette to the filament on the electrodeposition apparatus and electrolyzed for 20 minutes at 3.4 V.
- 2.7.5. The voltage is reduced to 3.0 V and 5  $\mu$ L of platinum DNS (5  $\mu$ g/mL) is added.
- 2.7.6. Electrolysis is continued for 20 minutes at 3.0 V.
- 2.7.7. With the plating voltage on at 3.0 V, the electrolyte is rinsed from the filament with deionized water.
- 2.7.8. The filament is removed from the plating apparatus and rinsed thoroughly with deionized water and finally with glass distilled acetone.

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2.7.9. The filament is first dried under a heat lamp for 10 minutes. The filament is then resistively heated to 350° C by running 1.25 amps current through the filament for 5 minutes while the heat lamp is still on.

- 2.7.10. The filament is placed into the filament carrier for insertion into the mass spectrometer as quickly as possible to prevent reabsorption of water onto the filament.
- 2.7.11. The mass spectrometer with the loaded samples is pumped down to a pressure of  $1-2 \times 10^{-6}$  torr in the source chamber and  $2-4 \times 10^{-9}$  torr in the analyzer.
- 2.7.12. The heating protocol for analysis of plutonium is as follows:

Approximate Time (Minutes)	Approximate Filament Temperature (°C)	Comments
0	1100	
2	1200	
4	1300	
6	1400	Begin search for <sup>242</sup> Pu peak
8	1450	Optimize ion source
10	1500	Instrument is tuned
12	1550	Start base line acquisition on bases of interest
20	1580	Data acquisition
30	1580	Data acquisition
60	1580+	Data acquisition should be complete

5. Describe the type of measurement system used, including a general description of its operation. Also indicate the type of analysis software utilized for any calculations and/or corrections applied to raw measurement data if applicable.

#### 1.0. TIMS Data Collection

Measurements are made on a single stage thermal ionization mass spectrometer which is housed in our clean room facilities. The end of the previous section describes the preparation of the sample before making measurements.

The following is a description of the protocol used for collecting data for the plutonium bioassay samples. The bioassay samples require the precise measurement of the plutonium isotope in the samples. The primary plutonium isotopes measured are <sup>239</sup>Pu and <sup>240</sup>Pu. When the signal or amount of <sup>239</sup>Pu is very low, it is not reasonable to spend time in trying to measure the <sup>240</sup>Pu. The

amount of <sup>239</sup>Pu is always larger than the amount of <sup>240</sup>Pu. This is reflected in the protocol that has been established for these measurements.

Baseline are run in all cases. Measurements will commence when the <sup>242</sup>Pu (the tracer) count rate exceeds 50,000 counts per second. Upper limit measurements for <sup>239</sup>Pu/<sup>242</sup>Pu ratio will continue until the 242.5 mass count rate falls below 1.5 counts per second. Real measurements will commence at that point.

If the <sup>239</sup>Pu/<sup>242</sup>Pu ratio is 3 x 10-5 or greater, the protocol will dictate a time symmetric measurement sequence: 1 block of <sup>239</sup>Pu/<sup>242</sup>Pu, 2 blocks of <sup>240</sup>Pu/<sup>242</sup>Pu, and two blocks of <sup>239</sup>Pu/<sup>242</sup>Pu. Typical collections of data to create a block are given in figures 1 and 2.

If the  $^{239}$ Pu/ $^{242}$ Pu is less than 3 x 10-5, then usually 4-5 blocks of  $^{239}$ Pu/ $^{242}$ Pu will be taken.

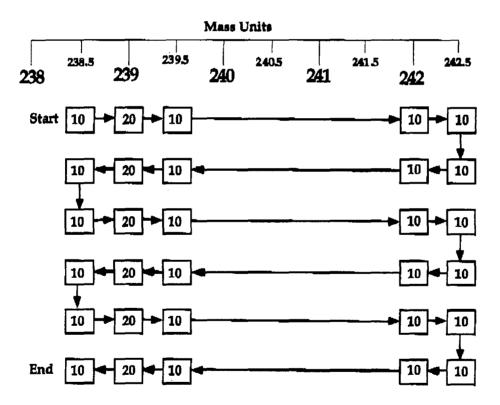


Figure 1. Measurement Sequence for Acquiring One Block of 239/242 Data.

Typical Sequence of Mass Spectrometric Measurements if 242/239 ratio is less than  $3 \times 10^{-5}$ . Numbers in blocks are typical 1-second counts at that mass region. The number of 1-second counts may vary.

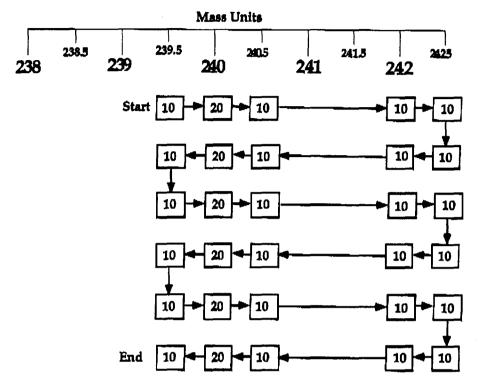


Figure 2. Measurement Sequence for Acquiring One Block of 240/242 Data.

Typical Sequence of Mass Spectrometric Measurements if 242/239 ratio is greater than  $3 \times 10^{-5}$ . Numbers in block are typical 1-second counts at that mass region.

6. Using actual measurement data, calibration factors, corrections, etc., give a sample calculation showing how the massic activity and uncertainty values reported in section 2 were determined. Indentify all values used, e.g., efficiency, calibration factors, mass, volume, decay corrections, etc.). Attach a separate sheet if necessary.

#### 1.0. TIMS Data Treatment

The following example is given for a bioassay sample calculation. Because the actual spreadsheets and calculations are extensive only pertinent portions of it are given to illustrate the steps of the calculations and associated statistics involved in the TIMS calculations.

#### This is not one of the samples reported in this report.

The count rates taken in each block are averaged and the background counts are subtracted. Five blocks of data are represented in Table I where the data are treated with regards to acceptance.

- 1.1. Column 1. These are the <sup>239</sup>Pu/<sup>242</sup>Pu ratios that have the backgrounds subtracted.
- 1.2. Column 2. This column has the corresponding standard deviations (SD) of the measured <sup>239</sup>Pu/<sup>242</sup>Pu ratios.
- 1.3. Column 3. The ratio divided by the standard deviation (SD) squared is the first element in determining a weighted average.
- 1.4. Column 4. The value 1/SD<sup>2</sup> is the weighting factor used for calculating the weighted average given at the bottom of the table with its standard deviation.
- 1.5. Column 5. The value of the [(average value individual value)/SD]2 is for the determined the reduced Chi Square value. This is determined as 1.836. The expected Chi Square value is 1.140. If the determined Chi Square value were 1.140 or less, then the all the data would be accepted with the average and standard deviation. Since this set of data does not meet this criterion, Chauvent's Criterion for rejection of data is used.
- 1.6. Column 6 through 10 are for the purpose of determining which data points may be rejected using the Chauvenet's Criterion.
- 1.7. Column 6. Starting at the bottom of column one the average of the last two samples are made and reported at the bottom of column 6. The average in the box above is for the three last entries. This is repeated until the top number is the average of all the values.
- 1.8. Column 7. The corresponding standard deviations are given in this column.
- 1.9. Column 8. This is the number of standard deviations the measured 239Pu/242Pu ratio varies from the ascending average.
- 1.10. Column 9. These are calculated Chauvenet's Criterion values.

Table III. One Block of TIMS Data for 299pu/342pu Ratio.

	Т		Т	Т	$\overline{}$	Т	$\top$	Т	Т	1	Т	Т	Т	Т	1	7	_	7		_	Т.	_	т
	We OK			Delete Point	TAKE TOTAL																		
Column 10	All Positive OK		7950	9000	0.449	0.548	0690	1.177	0.929	0.524	0.872	0.611	1.183	0.0%4	0.348	0.443	2						
Column 9	Ascending Numbe Chauvener's	Criterion	2.128	2.100	2.070	2038	2002	1.960	1.914	1.863	1.803	1.731	1.645	1.534	1383	1.150							
Column 8	Numbe	rofSD	-2525	30%	-1.621	-1.490	-1312	-0.783	-0.985	-1339	0.931	1.120	-0.462	0.570	-1.085	-0.707							
Column 7 Column	Ascending	S	5.179E-06	3.846E-06	1.819E-06	1.659E-06	1.537E-06	1.459E-06	1.487E-06	1.478E-06	1342E-06	1.341E-06	1.253E-06	1.398E-06	1.583E-06	9.931E-07							
Column 6	Ascending	Average	1.37UE-05	1.277E-05	1.185E-05	1.161E-05	1.138E-05	1.118E-05	1.105E-05	1.087E-05	1.0598-05	1.080E-05	1.110E-05	1.095E-05	1.122E-05	1.040E-05							
Column 5	(Ave-	x/SD)^2	8.494E+00	8.903E+00	1.007E+00	5.394E-01	3.911E-01	2.199E-02	4.843E-02	2132E-01	1.807E+00	1.543E+00	1.983E-02	7.336E-01	1.424B-01	1.734E-01	1.672E+00	Reduced	٦ ڳ	1.836	Expected	Vanie	1.140
Column 4	1/SD^2	-	_	5.503E+10	1243E+11	1.195E+11	1.872E+11	1.623E+11		2.658E+11	2.641E+11	2.181E+T1	2.543E+11	2265E+11	1.750E+11	2.378E+11	3.278E+11	-3	2808E+12				
Column 3	X/SDv2	_		1.358E+06	1.840E+06	1.682E+06		200	_	3.415E+06		2027E+06	2.969E+06	2300E+06	2250E+06	2.639E+06	3.178E+06	Σ=	3.357E+07				
Column 1 Column 2 Column 3 Column 4	Std Dev	_			_ 1	2.8984E-06		24823E-06		ı	1.9457E-06	1	1.9830E-06	1.0154E-05 2.1013E-06	23905E-06	2.0508E-06	1.7467E-06						
Column 1	239/242	Katho	2.6777E-05	24674E-05	1.4801E-05	1.4079E-05	1.3400E-05	1.2322E-05	1.2519E-05	1.2850E-05	9.3390E-06	9.2945E-06	1.1675E-05	1.0154E-05	12856E-05	1.1100E-05	9.6959E-06						

12



1.11. Column 10. The values in this column represent the difference of column 9, Chauvenet's Criterion and the absolute value of the number of standard deviations of column 8. The test has been constructed so that all negative values may be rejected. The "Deletion Point" is noted on the last negative value.

The data points are seen graphed in Figure 3.

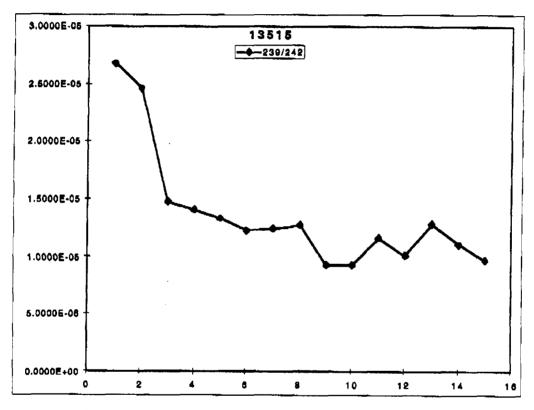


Figure 3. Plot of individual <sup>239</sup>Pu/<sup>242</sup>Pu values.

- 1.12. The process of calculating the weighted average is repeated with the first two points rejected. As expected the reduced Chi Square is 0.643 for the set of data and the expected value is 1.148. This yields an average of 1.149 x  $10^{-5} \pm 6.067 \times 10^{-7}$  (% SD = 5.28%), for this example.
- 1.13. The sample is then corrected for mass fraction (0.0011) yielding a mass corrected value of  $1.145 \times 10^{-5} \pm 6.067 \times 10^{-7}$  (5.28%).
- 1.14. Process blank contribution to the  $^{29}$ Pu is subtracted:  $(1.145 \times 10^{-5} \pm 6.067 \times 10^{-7}) (1.644 \times 10^{-7} \pm 2.154 \times 10^{-7}) = 1.129 \times 10^{-5} \pm 6.565 \times 10^{-5}$ .

Messer out undersion

- 1.15. The amount of tracer added at the beginning of the experiment was 1.050 g which contained 7.5245 x 1012 atoms 242Pu per gram of tracer. Uncertainty in this value is 0.25% and is not propogated in this calculation. Exactly 1.050 g solution was added initially. There are 7.5245 x 1012 atoms 242Pu per g solution; this is  $7.901 \times 10^{12}$  atoms <sup>242</sup>Pu added.
- 1.16. The number of <sup>259</sup>Pu atoms in the sample initially is:  $(1.129 \times 10^{-3} \pm 6.565 \times 10^{-3} \pm 6$  $10^{-7}$  atoms  $^{239}$ Pu/ $^{242}$ Pu) x (7.901 x  $10^{12}$  atom  $^{242}$ Pu) = 8.920 x  $10^{7} \pm 5.191$  x  $10^{6}$  atoms <sup>239</sup>Pu in the sample measured.
- 1.17. The half-life used for <sup>239</sup>Pu is 2.410 x 10<sup>4</sup> years. The decay constant,  $\lambda$ , in sec<sup>-1</sup> is  $9.118 \times 10^{-13}$ . The number of Bq in the sample measured is  $9.118 \times 10^{-13}$  $\sec^{-1} \times 8.922 \times 10^{7} \pm 5.191 \times 10^{6}$  atoms =  $8.133 \times 10^{5} \pm 4.734 \times 10^{6}$  Bq in the sample measured.
- 1.18. Remembering that the sample had 0.5 mL removed for a specific gravity measurement, the correction for the activity in the sample as received is  $8.133 \times$  $10^{-5} \pm 4.734 \times 10^{-6}$  Bq x (225.2 g as received/224.7 g sample measured) = 8.151 x  $10^{-5} \pm 4.745 \times 10^{-6}$  Bq in sample as received.
- 1.19. The amount of Bq/g sample is  $(8.151 \times 10^{-6} \pm 4.745 \times 10^{-6})$  Bq/225.2 g =  $3.619 \times 10^{-8} \pm 2.107 \times 10^{-9}$  Bq/g sample.
- 1.12. The values reported with 3 significant figures would be:

Total Activity in the Bottle:

 $8.13 \times 10-5 \text{ Bq}$ 

Massic Activity:

 $3.62 \times 10-8$  Bq/g sample

Uncertainty:

5.82% (1s)

7. The deadline for submitted report is May 9, 1997. Please address results and technical questions to:

Kenneth G.W. Inn

Phone: 301-975-5541

NIST

245/C114

Gaithersburg, MD 20899

Fax: 301-869-7682 email: kenneth.inn@nist.gov

14

- measurement pression

#### Donivan Porterfield, 01:38 PM 6/1/97 -, assessment of ORNL low-level

X-Sender: dporterfield@lims1.lanl.gov (Unverified)

Date: Sun, 01 Jun 1997 13:38:34 -0600

To: kenneth.inn@nist.gov

From: "Donivan Porterfield, LANL CST-3" <dporterfield@lanl.gov> Subject: assessment of ORNL low-level Pu in urine PE samples

Pat Brug requested that I send you this draft memo regarding our results from the special low-level plutonium in urine samples from ORNL.

The attached file should be in MS Word 6.0. Attachment Converted: C:\EUDORA\ENCL\CST-ACES.doc

Donivan Porterfield (505) 667-4710
Los Alamos National Laboratory (505) 665-5982 fax
MS K484, CST-3 (Analytical Quality and Chemical Information
Management)
Los Alamos, NM 87545 dporterfield@lanl.gov

To: Distribution

From: Donivan Porterfield, CST-3
Thru: Peggy Gautier, CST-3
Date: DRAFT (5/25/97)

Re: Summary of results from ORNL low-level plutonium in urine pilot study

CST Analytical Chemistry has participated in the Oak Ridge National Laboratory (ORNL) Bioassay Intercomparison study for several years. With the transition of routine plutonium in urine bioassay analyses from CST-9/TA-59 to CST-11/TA-48 CST-3 has continued the participation of Analytical Chemistry in this study. Three study samples are supplied on a quarterly basis for the following analytes and matrices and distributed as indicated:

<u>Analyte</u>	<u>Matrix</u>	<u>Capability</u>
Americium-241	Urine	CST-9/TA-59
Plutonium	Urine	CST-11/TA-48
Plutonium	Urine	CST-9/TA-59
Strontrium-90	Urine	CST-9/TA-59
Total Uranium	Urine	CST-9/TA-59
Tritium	Urine	CST-9/TA-59

With the addition of the thermal ionization mass spectrometry (TIMS) capability, ORNL suggested that they could supply us with a similar plutonium in urine samples but at a lower plutonium spike level. As a pilot ORNL offered to provide several samples of this type at no charge. This offer was accepted and ORNL prepared and shipped these samples to CST-3 for submission to CST-11 for analysis by alpha spectroscopy and TIMS. This memo is to report the results of the analysis of these supplied samples and invite input in the decision to participate on a regular basis in a low-level ORNL intercomparison study.

The reported results will be assessed on the basis of relative bias and relative precision as indicated in ANSI 13.30 (*Performance Criteria for Radiobioassay*), sections 4.3.2 and 4.3.3. These sections provide performance criteria of -0.25 to +0.50 for relative bias and <0.4 for relative precision.

The samples supplied by ORNL will be referenced with the CST-AC sample number since the ORNL sample identification used personal identification of the urine donors. In addition to the four samples provided that were spiked with plutonium-239 there were two samples spiked with plutonium-238. Since the plutonium activity of these samples was below that detectable by alpha spectroscopy and TIMS doesn't report plutonium-238 these results will not be evaluated in this memo. As well, since the plutonium-239 activity of this plutonium-238 spike is unknown, the plutonium-239 results for these two samples will not be assessed.

#### Plutonium-239 by TIMS

Sample ID	Known (aCi/sample)	Reported (aCi/sample)	Bias	Relative Bias	Relative Precision
97.01029	3040	3234	0.064		
97.01030	3070	4258	0.387		
				0.225	0.229
97.01033	12200	12490	0.024		
97.01034	12200	12700	0.041		
				0.032	0.012
			Overall	0.129	0.173

As indicated above all relative bias and relative precision values meet ANSI 13.30 acceptance criteria at the indicated spike levels.

On the basis of these results, ORNL feels assured in their ability to provide low-level plutonium in urine intercomparison samples. However, they have also indicated that they would not be comfortable in providing samples at any lower activity.

With regard to our future participation in a routine ORNL low-level intercomparison study we invite your input on the following issues:

- 1. That we would participate in low-level plutonium in urine intercomparison study on a quarterly basis. We envision that this low-level study would be offset from the current ORNL plutonium in urine intercomparison study.
- 2. That we would continue to participate in the current ORNL plutonium in urine study without change for assessment of both CST-9 and CST-11 alpha spectroscopy capabilities.
- 3. At current the plutonium spike standard used by ORNL doesn't have a know value for plutonium-240. Should we require the ORNL use a plutonium spike standard with a known plutonium-240 value?
- 4. With three samples in each study should we request that the activity of at least one sample be such that we could assess our plutonium-240 quantitation performance? If so, what activity level would be necessary? Or do we request samples with enhanced abundance of plutonium-240?

#### Distribution:

Dawn Lewis, ESH-12

Pat Brug, CST-3, MS K484
Peggy Gautier, CST-3, MS K484
Nancy Koski, CST-3, MS K484
Carolyn Macdonell, CST-3, MS K484
Jose Olivares, CST-9, MS K484
Edward Gonzales, CST-9, MS K484
Glenn Bentlley, CST-11, MS J514
Moses Attrep, CST-11, MS J514
Tim Benjamin, CST-11, MS J514
Donald Dry, CST-11, MS J514
Wes Efurd, CST-11, MS J514

```
Moses Attrep, 03:03 PM 8/6/97 +, Re: Intercomparison Results-LA
X-Sender: 098804@cstnt1.lanl.gov
Date: Wed, 6 Aug 1997 15:03:17 +0100
To: Ken Inn <kenneth.inn@nist.gov>
From: Moses Attrep <mattrep@lanl.gov>
Subject: Re: Intercomparison Results-LANL
Ken: Here is the value reported on the final revised report:
Sample 00.35880:
Total activity (Bq) in Each Bottle:
                                        2.04 E-05
                                9.36 E-08
Massic Activity (Bq/g):
                                184.3%
Uncertainty:
Hope this is what you need.
Moses
PS Did you get the forms for the visitor?
>Dr. Attrep:
>Could you please tell me, again, what value you got for #61,
00.35880? I've
>lost the value you gave me over the phone.
>Thanks,
>Ken
>PS: We got the visitor's forms. I used to have a "Q" clearance, but
>management here thought my job was low risk and removed my clearance.
>At 11:26 AM 6/5/97 +0100, you wrote:
>>Ken:
>>Thanks for talking with us the other day. I have attached the final
```

>>Thanks for talking with us the other day. I have attached the final >>results for the Yankee Atomic samples. As we indicated when talking with >>you the value of the one sample (#61, 00,35880) did change, but

>>you the value of the one sample (#61, 00.35880) did change, but checking

>>the calculations of the other one we found no change.

>>I have also attached some comments with the results.
>>

>>Donivan has looked through ANSI 13.30 and did not find the synthetic urine

>>recipe. We are still looking around. Meanwhile, I'd appreciate getting

Printed for Ken Inn <kenneth.inn@nist.gov>

#### Moses Attrep, 03:03 PM 8/6/97 +, Re: Intercomparison Results-LA

>>what was used in this study and compare it with the recipe we used.
>>
>>Thanks.
>>
>>Moses
>>
>>Attachment Converted: C:\EUDORA\ENCL\Yankee\_A.doc
>>Moses Attrep, Jr.
>>Los Alamos National Laboratory
>>MS J514
>>Los Alamos, NM 87545
>>505 667-0088
>>E-Mail: mattrep@lanl.gov
>>

Moses Attrep, Jr.
Los Alamos National Laboratory
MS J514
Los Alamos, NM 87545
505 667-0088
E-Mail: mattrep@lanl.gov

## Attachment VIII PNNL ICP-MS Report



902 Banelle Blvd P.O. Box 999 Richland, WA 99352

### Fax Cover Sheet

DATE: 6/11/97

TO: Ken Inn

FROM: Eric Wyse

PHONE: 301 975 5541

301 869 7682

PHONE: 376-3074

FAX: 376-7475

Number of pages including cover sheet:

Message

Ken - here's the data on the Sheets requested.

Some of the errors may be over-estimated - We can

Some of the errors may be over-estimated - We can

discuss later. I'll type up our procedure + analysis

4 get that out to you later this afternom.

I figured you could use this information first.

## Results of Measurement <sup>239/240</sup>Pu in Artificial Urine

Please use this data reporting form for the submission of analytical results. Twenty-five samples of <sup>239/240</sup>Pu spiked unstable artificial urine (> 10000 aCi/sample) have been provided for this study. Please analyze the total content of each bottle of sample, and report the individual measurement results. The reference date and time for your reported results is:

#### 12:00 noon EST. February 26, 1997

2. Report measurements in Bq'g' of solution. Report total combined standard uncertainty as 1s (%).

Sample Number	Total Activity (Bq) in each Bottle	Massic Activity (Bq'g <sup>-1</sup> )	Uncertainty (% 1s)
Puro 297 - 02	3.4 × 10 -5	1.7×10-7	49%
03	6.7 × 10 <sup>-5</sup>	3.2 × 10-7	49%
07	1 × 10-4	5 × 10 <sup>-7</sup>	80% (est.)
10	<   ×   0 <sup>-5</sup>	< 5 x  0 - ₹	
14	4.8 × 10 <sup>-5</sup>	2.3 × 10-7	30%
17	2 × 10 <sup>-5</sup>	9×10 <sup>-8</sup>	70%
23	2.3 × 10 <sup>-5</sup>	1.1 × 10 <sup>-7</sup>	67%
24	2.1 × 10 <sup>-5</sup>	9.4 × 10-8	40%
28	1.2 × 10 <sup>-4</sup>	5.5 × 10 <sup>-7</sup>	46%
30	<1 × 10 <sup>-5</sup>	< 5 × 10 <sup>-8</sup>	
34	<2 × 10-5	< 1 × 10 <sup>-7</sup>	
38	<2 × 10-5	<   × 10 <sup>-₹</sup>	
43	< 2 × 10-5	< 1 × 10-7	
49	7.1 × 10 <sup>-5</sup>	3.2×10 <sup>-7</sup>	30%
55	7×10 <sup>-6</sup>	3 × 10-8	1007.
56	1.1 × 10-4	5.1 × 10 <sup>-7</sup>	277

Kinn/dosehpu

PuRo 297 - 64	2.5×10-5	1.2×10 <sup>-7</sup>	40%
67	3.7 × 10-5	1.6 × 10 <sup>-7</sup>	50%
69	4.6 × 10 <sup>-5</sup>	2.0 × 10-7	28%
72	2.8 × 10.5	1.3×10-7	112%
76	2.3 × 10-5	1.0 × 10-7	59%
88	7.3 × 10 <sup>-5</sup>	3.5 × 10 <sup>-7</sup>	30%
94	7.8 × 10-5	3.6×10-7	47%
97	1.1 × 10-4	5.0 × 10-7	35%
. 99	8.0 × 10-5	3.9 × 10-7	31%

3. State the ±1s "standard uncertainty" components (random and systematic) which comprise the combined standard uncertainty. These may include, but are not limited to the following:

Uncertainty due to impurity corrections = \_\_\_\_\_\_%.

Uncertainty due to tracer calibration = \_\_\_\_\_\_\_%.

Uncertainty due to spectral interferences = 20 %.

4 Others; please describe.

Preperrors Should be corrected by use of isotopic tracer

Tracer was not calibrated for This run. Previous calibrations have indicated very close correlation with our Pu-239 std on a mass basis. Error conservatively estimated at 10%.

Varied depending on concentration. Attributed exclusively to background signal moise ratio.

Precision between replicate runs; varied - averaged ~10%.

Blank - variability in 239/245 ratio in blanks.

Kinn/doeahpu

6. Using actual measurement data, calibration factors, corrections, etc., give a sample calculation showing how the massic activity and uncertainty values reported in section 2 were determined. Identify all values used, e.g., efficiency, calibration factors, mass, volume, decay correction, etc.). Attach a separate sheet if necessary.

## Errors

- a. Tracer calib est. 10%
- b. Grav. measurement est. 1%

C. Bkg/spectral: 
$$3 \cdot \sqrt{89} = 28 \text{ cts} \pmod{1}$$
  
Net 239 ct = 278-89 = 189 ct  
 $\frac{28}{189} = 15\%$ 

e. Precision: 
$$34.5 (Run 2)$$
  
 $30 (Run 1)$   
 $\overline{Ave} = 32 = 3$ 

Total = 
$$\sqrt{(10)^2 + (1)^2 + (15)^2 + (23)^2 + (10)^2}$$
 = 31%  
From Gravinstin BKG BLK Prices in

7. The deadline for submitted results is May 16, 1997. Please address results and technical questions to:

Kenneth G.W. Inn NIST 245/C114 Gaithersburg, MD 20899

Phone: 301-975-5541
Fax: 301-869-7682

email: kenneth.inn@nist.gov

Kana/dosehpu



902 Banelle Blvd P.O. Box 999 Richland, WA 99352

## Fax Cover Sheet

DATE: 6/11/97

TO: Ken Inn NIST

FROM: Eric Wyse

PHONE: 301 975 5541

301 869 768.2 FAX:

PHONE: 376-3074

376-7475 FAX:

Number of pages including cover sheet: Message

Ken- I noticed that the Roults page indicates

239 Pu AND 240 Pu. I seem to remember noticing and inquiring about this earlier, but I forget what the answer was. The reported results are ONLY for Pu-239. We could have looked for 240, but unless there was a similar Mars of that isotopes, we probably wouldn't be based to see it. Once again, the activities reported were converted directly from the mass obtained for Ru-239 - it DOES NOT account for activity due to Ru-240. Please call with any questions.

## Results of Measurement <sup>239</sup>Pu in Artificial Urine: Questions 4 and 5 June 11, 1997

4) Sample preparation started on May 19. Each sample was transferred as quantitatively as possible to a tared 400 mL beaker and weighed. A 30 mL concentrated nitric acid aliquot was then added to the sample container; it was swirled around the walls for a few seconds. then transferred to the 400 mL sample beaker. To the acidified sample, 100µL of a 116 pg/mL <sup>244</sup>Pu solution was weighed and added as a tracer and internal standard. The acidified samples were digested by heating at 90°C for ~2 hours. The plutonium was then coprecipitated with calcium phosphate. The precipitate was isolated and redissolved and wet-ashed with nitric acid and hydrogen peroxide. After a clear solution was obtained, the residue was dissolved in ~3 mL 2M HNO<sub>3</sub>. A microcolumn of TEVA-Spec™ resin was prepared by passing a resin/water slurry through a syringe filter. The microcolumn is first conditioned with 2 mL 2M HNO, before passing the dissolved residue. After passing the sample, the column is then rinsed with 2 mL 2M HNO<sub>3</sub>, then reconditioned with 3 mL 6M HCl, and finally eluted with 2 mL deionized water into 10 mL plastic test tubes. All samples were eluted by May 27.

IN 68 stale from

On May 29, the samples test tubes were placed in a hot water bath to reduce sample volume by evaporation. The target volume was 0.5 mL. By COB May 30, the volume had only been reduced down to just under 1 mL. The samples were removed from the heat and left uncovered over the weekend. By June 2 the volume had reduced to the target value of ~0.5 mL. Instrument sensitivity and background were both fairly good when the first sample analysis started on June 2. More than half of the samples were completed on June 2. The samples were covered with Parafilm overnight. Instrument sensitivity waned considerably after continuing the batch run on June 3. Samples were re-covered while instrument maintenance was performed to improve instrument response. Performance returned on

## Pu in urine, Questions 4 and 5 (cont.)

6/11/97

June 6. The second analysis was started Friday (6/6), but other instrument problems persisted on Friday and over the weekend. 'Kinks' were finally ironed out on Monday, June 9 (nebulizer cleared, good sensitivity, low background), and the analysis was completed by Monday evening.

5) Samples were analyzed on a VG Plasmaquad II+ using the 'S-option' enhanced-sensitivity interface. A membrane desolvation microconcentric nebulizer (MCN-6000 from Cetac) self-aspirating at ~20µL/min was used for sample introduction. A 10 minute data acquisition in peak-hopping mode (9 channels per peak) was made for each sample.

Calculations were done manually ('hand calculations') based on the peak integrals obtained for m/z 239 (isotope of interest), 244 (tracer), and 245 (designated background). The <sup>239</sup>Pu concentration was determined by comparing the net counts of m/z 239 with the counts obtained at m/z 244 for a known quantity of Pu. The 238 peak was also monitored to indicate excessive uranium concentrations. The uncertainty values were calculated as described on the Results report (question 6). An Excel 5.0 spreadsheet was used to facilitate all calculations.

## IV.

## MEASUREMENT RESULTS and DATA ANALYSIS

## Mean, Standard Deviation and Bias

The deviations from the NIST values for each determination, the average deviation from the NIST values, and the standard deviation were determined for the data that survived the outlier tests. Spreadsheets 1, 2, 3 and 4 report the measurement results for the participating laboratories. Table 4 summarizes the determination of the Total Propagated Uncertainties (K=1).

The spreadsheets list the following information:

ID Sample Identification Number

Avg/1s Mean value and 1 standard deviation of the

reported values

Target solution concentration in aCi/sample

Sample Mass of sample solution

Known NIST <sup>239</sup>Pu concentration value of the sample

solution as nBq/g and nBq/sample

Sigma1% 1 sigma total propagated uncertainty of the

NIST value in percent

Measured Reported <sup>239</sup>Pu per sample as nBg/sample and

percent sigma total propagated uncertainty

Bias% Percent difference between the NIST and

reported nBq/sample value

Notes Reason for not including the measured value

in the assessment

Measured Reported <sup>239</sup>Pu per sample as nBg/g and

percent sigma total propagated uncertainty

Bias% Percent difference between the NIST and

reported nBq/g value

## Spreadsheets 1-4 Measurement Results and Data Analysis

PNL-ICPMS		∢	Ω.	ပ	۵	ш	ı	g	I	_	7	×	لد	Σ
Particular   Par														
a CiviSample g         nBq/g         nBq/Sample Sigma1%         nBq/Sample Sigma1         nBq/Sample Sigma1%         nBq/Sample Sigma1         nBq/Sample Sigma1		; ;	1	SampleMass	Known	:		Measured		Rias%	Notes	Measured		Risc%
18 BLK         207         0         0         *.3800         250         Low CY           46 BLK         204.45         0         0         *.3800         31.3         Low CY           46 BLK         204.45         0         0         0         0         40.0         41.3           28 BLK         105 BLK         125.65         0         0         0         40.0         41.3           100 BLK         228 BL         100         2215.7         18.5114         4180.25588         0.5         3400         7.3         14.85           100 BLK         228 LL         18.5114         4180.25588         0.5         3600         7.1         22.05           56 100         222.2         18.5114         4118.7858         0.5         3600         7.1         32.05           56 100         222.2         18.5114         4118.7858         0.5         3600         7.1         32.05           56 100         222.2         18.5114         4118.7858         0.5         3600         7.1         32.05           57 100         220         22.0         22.0         22.0         7.1         32.0           58         100         222.1 </td <td></td> <td><u>_</u></td> <td>Sample</td> <td>·</td> <td>nBq/g</td> <td>nBq/Sample</td> <td></td> <td></td> <td>1</td> <td>+-</td> <td>2</td> <td>nBa/a</td> <td>Sigma1%</td> <td>4</td>		<u>_</u>	Sample	·	nBq/g	nBq/Sample			1	+-	2	nBa/a	Sigma1%	4
46 BLK         204.45         0         0         *.3800         31.3         Low CY           100 BLK         195.65         0         0         200         31.3         Low CY           100 BLK         195.85         0         0         0         200         31.3         Low CY           100 BLK         228.85         0         0         0         220         17.5         Low CY           101 BLK         228.85         0         0         0         220         17.5         Low CY           101 BLK         228.85         0         0         0         220         17.1         18.514         418.5258         0.5         2800         7.1         18.514         19.25         19.65         19.02 </td <td></td> <td>18</td> <td></td> <td>207</td> <td>1</td> <td>0</td> <td>4</td> <td></td> <td></td> <td></td> <td></td> <td>0.3</td> <td>+</td> <td></td>		18		207	1	0	4					0.3	+	
71 BLK         2015         0         0         800         313         Continuo           100 BLK         195.65         0         0         600         417         7           100 BLK         228.85         0         0         25         1161.807         7           101 BLK         228.85         0         0         0         7.3         14.85           102 BLK         226.4         18.5114         3992.90888         0.5         3400         7.3         14.85           100 C220.4         18.5114         4150.25588         0.5         360         7.1         132.02           56 C100         222.2         18.5114         4118.23308         0.5         2800         7.1         132.02           57 C100         222.2         18.5114         4118.233308         0.5         2800         7.1         19.62           29 C50         220.0         18.5114         4118.233308         0.5         3260         7.1         1.0           21 C50         46.2934         10260.9321         0.5         2800         2.1         1.6         1.0           25 C50         271.2         46.2934         1056.24888         0.5         28400 </td <td></td> <td>94</td> <td>BLK</td> <td>204.45</td> <td>0</td> <td></td> <td></td> <td>1</td> <td></td> <td></td> <td>Low CY</td> <td>* 19</td> <td></td> <td>1</td>		94	BLK	204.45	0			1			Low CY	* 19		1
100 BLK   195.65		7	BLK T	201.5	0			900	31.3			4		
100 BLK         228.85         0         0         200         75           unith         100         215.7         18.5114         4150.25588         0.5         3400         73         -14.85           36         100         224.2         18.5114         4150.25588         0.5         9600         7         -14.85           36         100         224.2         18.5114         4170.25588         0.5         9600         7         -14.85           56         100         222.2         18.5114         4173.23308         0.5         9600         7         -1-8.52           56         100         222.2         18.5114         4173.23308         0.5         9600         7         -1-8.52           56         100         222.2         18.5114         4173.23308         0.5         3275         5.196076         -19.62           26         250         221.6         46.2934         10260.9321         0.5         9000         2.1.26         -1.26           27         250         271.6         46.2934         10073.4438         0.5         800         2.1.26         -1.26           28         250         217.6         46.2934		92	BLK	195.65	0	!		900	417			6		
uniti)         100         215.7         18.514         3992.90898         0.5         3400         7.3 - 14.85           36         100         224.2         18.514         4150.25588         0.5         3400         7.6 - 19.12           56         100         222.4         18.514         4118.7865         0.5         3300         7.6 - 19.12           65         100         222.5         18.514         4079.91286         0.5         2800         7.1 - 32.02           75         100         222.2         18.514         4118.7865         0.5         2800         7.1 - 19.12           26         250         221.6         46.2934         10260.9321         0.5         9000         2.12.48           27         250         221.6         46.2934         10260.9321         0.5         8000         2.12.29           28         250         221.6         46.2934         9506.34969         0.5         8000         2.15.4         46.2934         9506.34969         0.5         8000         2.15.6         46.2934         9957.71034         0.5         8800         2.15.6         46.2934         9957.71034         0.5         8800         2.15.6         46.2934         9957.7103		18	BLK	228.85	0			200	75			0.7		
unit)         100         2215.7         18.5114         3992.90898         0.5         3400         7.3         14.85           36         100         224.2         18.5114         4190.25588         0.5         9600         7.1         32.02           56         100         220.4         18.5114         4118.7865         0.5         3600         7.1         32.02           65         100         222.2         18.5114         4118.7865         0.5         3600         7.1         32.02           75         100         222.2         18.5114         4118.7865         0.5         360         7.1         32.02           76         100         222.2         18.5114         4118.7865         0.5         3275         5.196076         19.62           20         250         221.65         46.2934         10073443         0.5         800         2.6         19.62           22         250         221.6         46.2934         10073443         0.5         800         2.6         1.6           28         250         21.6         46.2934         10073443         0.5         28400         0.5         1.6         1.6           44		Avg/1sm						25	1181.807			-0.025	-5931 55	
16         100         215.7         18 5114         3992 90898         0.5         3400         7.3         14.86           36         100         2242         18 5114         4150.2568         0.5         3300         7.6         19.12           56         100         222.2         18 5114         4113.23308         0.5         3300         7.6         19.12           75         100         222.2         18 5114         4113.23308         0.5         3600         6.9         12.248           75         100         222.2         18 5114         4113.23308         0.5         3200         7.1         12.28           22         250         221.65         46.2934         10260.9321         0.5         8000         2.8         12.28           22         250         217.6         46.2934         10260.9321         0.5         8600         2.8         10.7           32         250         217.6         46.2934         10260.9321         0.5         8600         2.8         10.7           41         800         220.4         46.2934         10260.9321         0.5         8600         2.8         10.7           52 <td< td=""><td>!</td><td>sm(nBq/unit)</td><td></td><td></td><td></td><td></td><td></td><td></td><td>295.4516</td><td></td><td></td><td></td><td>Ļ.</td><td></td></td<>	!	sm(nBq/unit)							295.4516				Ļ.	
36         100         224.2         18.5114         4150.25588         0.5         *9600         7.6         19.12           56         100         220.4         18.5114         4079.91256         0.5         3300         7.6         19.12           65         100         222.2         18.514         4118.7885         0.5         2800         7.1         -22.02           75         100         222.2         18.514         4118.7885         0.5         2800         7.1         -22.02           26         250         222.6         18.514         4118.7885         0.5         3275         5.196076         19.62           29         250         221.65         46.2934         10260.9321         0.5         9000         2.8         -10.71           29         250         221.65         46.2934         10273.4438         0.5         8500         5.1-10.71           54         250         212.9         46.2934         10273.4438         0.5         8800         2.1-10.71           55         250         212.9         46.2934         10273.4438         0.5         8800         2.8-10.71           54         250         215		16		215.7	18.5114	3992.90898		3400		+		16	-	-13 57
56         100         220.4         185114         4079.91256         0.5         3300         7.6         19.12           65         100         222.5         18.5114         4118.7865         0.5         2800         7.1         3202           75         100         222.2         18.5114         4118.7865         0.5         2800         7.1         3202           26         250         221.65         46.2934         10260.9321         0.5         9000         2.8         12.29           29         250         205.35         46.2934         10260.9321         0.5         8000         2.8         1.0.71           32         250         205.36         46.2934         10073.4438         0.5         8000         2.8         1.0.71           84         250         212.9         46.2934         10073.4438         0.5         8000         2.8         1.0.71           85         250         215.1         46.2934         10073.4438         0.5         8600         2.8         1.0.71           86         250         215.1         46.2934         10073.4438         0.5         8680         2.8         1.0.71           86		98		224.2	18.5114	4.	0.5	_			Outlier?	*43		
65         100         222.5         18.5114         4118.7865         0.5         2800         7.1         -32.02           75         100         222.2         18.5114         4113.23308         0.5         3600         6.9         12.48           26         250         221.65         46.2934         10260.9321         0.5         9000         2.8         -12.29           29         250         205.35         46.2934         9606.34969         0.5         7700         2.8         -12.29           34         250         212.9         46.2934         965.86486         0.5         8800         2.8         -10.71           85         250         212.9         46.2934         965.86486         0.5         8800         2.8         -10.71           85         250         212.9         46.2934         965.86486         0.5         8800         2.8         -10.71           86         250         215.1         46.2934         965.86486         0.5         8680         2.8         -10.71           86         250         215.1         46.2934         965.71034         0.5         8680         2.8         -10.71           81		58		220.4	18.5114	4079.91256	0.5	3300	7.6				7.6	-1897
75         100         222.2         18.5114         4113.23308         0.5         3600         6.9         12.48           26         25.0         221.65         46.2934         10260.9321         0.5         9000         2.8         -12.29           29         25.0         205.35         46.2934         10260.9321         0.5         8500         2.8         -12.29           29         25.0         205.35         46.2934         10073.4438         0.5         8500         2.8         -12.29           32         25.0         212.9         46.2934         10073.4438         0.5         8800         2.8         -10.71           85         250         215.1         46.2934         9957.71034         0.5         8600         2.8         -10.71           86         250         215.1         46.2934         9957.71034         0.5         8600         2.8         -10.71           86         250         215.1         46.2934         9957.71034         0.5         8600         2.8         -10.71           86         250         215.1         46.2934         9957.71034         0.5         28900         0.9         -12.64		65	:	222.5	18.5114		0.5	2800	7.1			12		+
26         250         221.65         46.2934         10260.9321         0.5         3275         5.196076         -19.62           26         250         221.65         46.2934         10260.9321         0.5         9000         2.8         -12.29           29         250         221.65         46.2934         956.34969         0.5         7700         2.6         -19.62           34         250         217.6         46.2934         9855.86486         0.5         8800         2.8         -19.62           35         250         217.6         46.2934         9857.71034         0.5         8800         2.8         -15.62           44         800         208.25         148.368         31268.56         0.5         28400         0.9         -8.084           5         800         210.75         148.368         31268.56         0.5         28300         0.9         -8.084           5         800         210.75         148.368         31261.1376         0.5         28300         0.9         -8.084           81         800         210.75         148.368         3196.9464         0.5         28900         0.9         -7.397 <td< td=""><td></td><td>75</td><td></td><td>222.2</td><td>18.5114</td><td>4113.23308</td><td>0.5</td><td>3600</td><td>6.9</td><td></td><td></td><td>16</td><td></td><td>┺-</td></td<>		75		222.2	18.5114	4113.23308	0.5	3600	6.9			16		┺-
26         250         221.65         46.2934         10260.9321         0.5         9000         2.8         -12.29           29         250         205.35         46.2934         9506.34969         0.5         7700         2.8         -1.9           32         250         217.6         46.2934         9506.34969         0.5         8800         2.8         -1.9           54         250         212.9         46.2934         9506.34969         0.5         8800         2.8         -1.9           54         250         212.9         46.2934         9855.8486         0.5         8800         2.8         -1.071           85         250         215.1         46.2934         9855.8486         0.5         8800         2.8         -1.071           44         800         216.7         48.386         31281.7134         0.5         8800         2.8         -1.5601           54         800         210.7         148.368         31281.36         0.5         28400         0.9         8.71           81         800         214.8         148.368         31281.33         0.5         28900         0.15         2.71           81 <t< td=""><td></td><td>Avg/1sm</td><td></td><td></td><td></td><td></td><td></td><td>3275</td><td>5.196076</td><td></td><td></td><td>14.75</td><td>6.416846</td><td>+ +</td></t<>		Avg/1sm						3275	5.196076			14.75	6.416846	+ +
29         250         205.35         46.2934         9506.34969         0.5         7700         2.6         -19           32         250         217.6         46.2934         10073.4438         0.5         8800         2.8         -10.71           85         250         215.1         46.2934         9855.86486         0.5         8800         2.7         -5.601           85         250         215.1         46.2934         9857.71034         0.5         8800         2.7         -5.601           86         250         215.1         46.2934         9957.71034         0.5         8800         2.7         -5.601           44         800         208.25         148.368         31268.556         0.5         31300         0.9         -8.084           5         800         210.75         148.368         31261.1376         0.5         28300         0.9         -8.472           87         800         214.8         148.368         31973.304         0.5         28900         1.56282         -8.231           87         1500         213.45         277.747         59285.0972         0.5         28900         0.4         -5.239		58		221.65	46.2934	10260.9321		0006	2.8	-12		40	2.8	-13.59
32         250         217.6         46.2934         10073.4438         0.5         8500         5.6         -15.62           54         250         212.9         46.2934         9855.86486         0.5         8800         2.8         -10.71           85         250         215.1         46.2934         9857.71034         0.5         8680         2.7         -5.601           44         800         208.25         148.368         30897.636         0.5         82400         0.9         -8.084           52         800         210.75         148.368         31268.556         0.5         28300         0.9         -8.084           54         800         210.75         148.368         31268.556         0.5         29200         0.9         -8.084           87         800         214.8         36         31869.4464         0.5         29200         0.7         -8.376           87         800         215.5         148.368         31973.304         0.5         29200         0.7         -8.376           87         1500         213.45         277.747         58674.0538         0.5         58900         0.6         -7.397           80 <td></td> <td>29</td> <td></td> <td>205.35</td> <td>46.2934</td> <td>9506.34969</td> <td>0.5</td> <td></td> <td>2.6</td> <td></td> <td></td> <td>38</td> <td></td> <td>+</td>		29		205.35	46.2934	9506.34969	0.5		2.6			38		+
54         250         212 9         46.2934         9855.86486         0.5         8800         2.8         10.71           85         250         215.1         46.2934         9957.71034         0.5         8680         2.7         -5.601           44         800         208.25         148.368         30897.636         0.5         28400         0.9         -8.084           52         800         210.75         148.368         31268.556         0.5         31300         0.9         -8.084           74         800         210.7         148.368         31268.556         0.5         28300         0.9         -8.084           87         800         215.5         148.368         31973.304         0.5         28900         0.7         -8.376           87         800         213.45         277.74         59285.0972         0.5         28900         0.15.6282         8.261           57         1500         213.45         277.74         59285.0972         0.5         58900         0.4         -5.239           70         1500         228.15         277.74         60298.873         0.5         55900         0.4         -5.239           <		32		217.6	46.2934		0.5		5.6	+		39		+
85         250         215.1         46.2934         9957,71034         0.5         9400         2.7         -5.601           44         800         208.25         148.368         30897,636         0.5         28400         0.9         -8.084           52         800         210.75         148.368         31268,556         0.5         28300         0.9         -8.084           74         800         210.7         148.368         31261,1376         0.5         28300         0.9         -8.472           87         800         215.5         148.368         31969,4464         0.5         29200         0.7         -8.376           87         800         213.45         148.368         31963,304         0.5         29800         1.156282         -8.261           35         1500         213.45         277.747         59285,0972         0.5         54900         0.5         7.397           57         1500         228.15         277.747         63287,9781         0.5         55900         0.4         -5.239           70         1500         221.1         277.747         61465,4111         0.5         57900         0.4         -7.295		3		212.9	46.2934		0.5		2.8	-10.71		41.5		·
44         800         208.25         148.368         30897.636         0.5         8680         3.286945         -12.64           52         800         210.75         148.368         31268.556         0.5         *31300         0.9         -8.084           74         800         210.75         148.368         31261.1376         0.5         *31300         0.9         -8.084           81         800         210.7         148.368         31261.1376         0.5         28300         0.9         -8.77           87         800         215.5         148.368         31963.464         0.5         29200         0.7         -8.376           87         1500         213.45         148.368         31973.304         0.5         28900         1.156282         -8.261           57         1500         211.25         277.747         59285.0972         0.5         55800         0.4         -5.239           70         1500         221.3         277.747         60298.8737         0.5         55900         0.4         -7.295           84         1500         221.3         277.747         61465.4111         0.5         55900         0.4         -7.295		85		215.1	46.2934	9957.71034	0.5		2.7			4	2	+
44         800         208.25         148.368         30897.636         0.5         28400         0.9         -8.084           52         800         210.75         148.368         31268.556         0.5         *31300         0.9         -8.084           74         800         210.7         148.368         31261.1376         0.5         28300         0.7         -8.376           87         800         216.5         148.368         31869.4464         0.5         29200         0.7         -8.376           87         1500         215.5         148.368         31973.304         0.5         28900         1.156282         -8.261           35         1500         213.45         277.747         59285.0972         0.5         28900         1.156282         -8.261           57         1500         211.25         277.747         59285.0972         0.5         55800         0.4         -5.239           70         1500         228.15         277.747         63367.9781         0.5         55900         0.4         -7.295           84         1500         221.3         277.747         61465.4111         0.5         57900         0.3         -7.295		Avg/1sm					0.5		3.286945			40.5	2.5896	-12.51
52         800         210.75         148.368         31268.556         0.5         *31300         O.9         -9.472           74         800         210.7         148.368         31261.1376         0.5         28300         0.9         -9.472           81         800         214.8         148.368         31973.304         0.5         29200         0.7         -8.376           87         800         215.5         148.368         31973.304         0.5         29700         0.7         -8.376           87         1500         215.5         148.368         31973.304         0.5         28900         1.156282         -8.261           35         1500         213.45         277.747         59285.0972         0.5         54900         0.4         -5.239           70         1500         211.25         277.747         58674.0538         0.5         55800         0.4         -5.239           70         1500         228.15         277.747         63367.9781         0.5         55900         0.4         -7.295           84         1500         221.3         277.747         61465.4111         0.5         57900         0.3         -7.295		4		208.25	148.368	30897.636		28400	0.0	_		136	60	-8 336
74         800         210.7         148.368         31261.1376         0.5         28300         0.9         9.472           81         800         214.8         148.368         31963.304         0.5         29200         0.7         8.376           87         800         215.5         148.368         31973.304         0.5         28900         0.1         8.771           35         1500         213.45         277.747         59285.0972         0.5         54900         0.5         7.397           57         1500         211.25         277.747         58674.0538         0.5         55800         0.4         5.239           70         1500         228.15         277.747         63367.9781         0.5         55900         0.4         -8.313           79         1500         221.1         277.747         61465.4111         0.5         57900         0.3         5.801           84         1500         221.3         277.747         61465.4111         0.5         57900         0.3         5.801           84         1500         221.3         277.747         61465.4111         0.5         57900         0.3         5.801 <td< td=""><td></td><td>52</td><td></td><td>210.75</td><td>148.368</td><td></td><td>0.5</td><td>4</td><td></td><td></td><td>Outlier</td><td>*149</td><td></td><td>i  </td></td<>		52		210.75	148.368		0.5	4			Outlier	*149		i 
81         800         214.8         148.368         31869.4464         0.5         29200         0.7           87         800         215.5         148.368         31973.304         0.5         29700         0.8           35         1500         213.45         277.747         59285.0972         0.5         54900         1.156282           57         1500         211.25         277.747         58674.0538         0.5         55600         0.4           70         1500         228.15         277.747         63367.9781         0.5         55900         0.4           79         1500         221.3         277.747         61465.4111         0.5         57900         0.3           84         1500         221.3         277.747         61465.4111         0.5         55900         0.3		74		210.7	148.368		0.5	28300	0.0			134	60	-9 684
87         800         215.5         148.368         31973.304         0.5         29700         0.8           35         1500         213.45         277.747         59285.0972         0.5         54900         1.56282           70         1500         211.25         277.747         58674.0538         0.5         55600         0.4           79         1500         228.15         277.747         60298.8737         0.5         55900         0.4           79         1500         221.1         277.747         61465.4111         0.5         55900         0.4           84         1500         221.3         277.747         61465.4111         0.5         55900         0.3           84         1500         221.3         277.747         61465.4111         0.5         55900         0.3		8		214.8	148.368	31869.4464	0.5		0.7		;	138		+
35       1500       213.45       277.747       59285.0972       0.5       28900       1.156282         57       1500       211.25       277.747       59285.0972       0.5       55800       0.4         70       1500       228.15       277.747       638674.0538       0.5       55800       0.4         79       1500       217.1       277.747       60298.8737       0.5       55900       0.4         84       1500       221.3       277.747       61465.4111       0.5       57900       0.3         84       1500       221.3       277.747       61465.4111       0.5       55900       0.3		87		215.5	148.368	31973.304	0.5		0.8	į .	j	138		
35         1500         213.45         277.747         59285.0972         0.5         54900         0.6           57         1500         211.25         277.747         58674.0538         0.5         55600         0.4           70         1500         228.15         277.747         63367.9781         0.5         58100         0.4           79         1500         217.1         277.747         60298.8737         0.5         55900         0.4           84         1500         221.3         277.747         61465.4111         0.5         57900         0.3           84         1500         221.3         277.747         61465.4111         0.5         56480         1.137011		Avg/1sm					0.5		-			136	0.600385	<del></del>
57         1500         211.25         277.747         58674.0538         0.5         55600         0.4           70         1500         228.15         277.747         63367.9781         0.5         58100         0.4           79         1500         217.1         277.747         60298.8737         0.5         55900         0.4           84         1500         221.3         277.747         61465.4111         0.5         57900         0.3           84         1500         221.3         277.747         61465.4111         0.5         56480         1.137011		35	; ;	213.45	277.747	59285.0972	0.5	54900	0.5			257	0.5	-7.47
70     1500     228.15     277.747     63367.9781     0.5     58100     0.4       79     1500     217.1     277.747     60298.8737     0.5     55900     0.4       84     1500     221.3     277.747     61465.4111     0.5     57900     0.3       9     60.5     66.486.4111     0.5     66.480     1.137011		22		211.25	277.747	58674.0538	0.5		0.			263		↓_
79         1500         217.1         277.747         60298.8737         0.5         55900         0.4 -7           84         1500         221.3         277.747         61465.4111         0.5         57900         0.3 -5           84         1500         221.3         277.747         61465.4111         0.5         56480         1.137011 -6		22		228.15	277.747		0.5		0.4			255	4.0	-8.19
84 1500 221.3 277.747 61465.4111 0.5 57900 0.3 0.5 56480 1.137011		79		217.1	277.747		0.5		0.4	7		257	4.0	<u></u>
0.5 56480 1.137011				221.3	277.747	61465.4111	0.5		0.3			262	0.3	-5.67
		Avg/1sm			:		0.5		1.137011	-6.809		258.8	0.603574	-6.822

С	S	T	U	V	W	X	Y	Z	AA
3	NOSM _	Meas						AccCrit	Pass/Fa
4		nBq/g							
5		-19		Regressio	n Output:				
6	1		Constant			-0.025			
7	-0.29		Std Err of			1.08901			
8	0.29	<del></del>	R Square			0.910113	0.953999	>0.868	Pass
9	1	3	No. of Ob	servations		4		·	
10				of Freedom		2		·	
11	x,stds,del	-0.025	2.965777						
12		· · · · · · · · · · · · · · · · · · ·	X Coeffic		3.328106				
13			Std Err of	Coef.	0.739575	·			+
14		<b></b>		<del></del>					!
15	1_	12		Regressio	n Output:				
16	-0.29		Constant			14.75			
17	0.29		Std Err of			1.063439			
18	1		R Square			0.789599	0.888594	>0.868	Pass?
19		43		servations		4			
20				of Freedom		2			
21_	x,stds	14.75	<del></del>	-20.3194		•			
22			X Coeffic	ient(s)	1.9786				
23			Std Err of	Coef.	0.722209				
24									
25	-1.13			Regressio	n Output:				
26	-0.49		Constant			-14.7365			
27	. 0		Std Err of			0.201057			
28	0.49	41.5	R Square	d		0.960029	0.979811	>0.879	Pass
29	1.13	44	No. of Ob	servations		5			
30		: L	Degrees of	of Freedom		3			
31	x,stds	40.5	2.345208	-12.5145					:
32			X Coeffic	ient(s)	0.363864				
33			Std Err of	Coef.	0.042865				
34									
35	1		İ	Regressio	n Output:				
36	-0.29	136	Constant			136			
37	0.29	136	Std Err of	Y Est		0.557049			
38	1		R Square			0.922424	0.960429	>0.868	Pass
39_		149	+	servations		4			
40				of Freedom		2			
41	x,stds_	138.6	5.98331	-6.58363				·	
42		•	X Coeffic		1.844848				
43	<u> </u>		Std Err of	f Coef.	0.378306			·	
44	· · · · · · · · · · · · · · · · · · ·	<del>1</del>	•					·	
45	-1.13			Regressio	n Output:		•		i
46	-0.49		Constant			-60.9347			
47	0		Std Err o		•	0.330993			
48	0.49	<del></del>	R Square				0.944283	>0.879	Pass
49	1.13	263	No. of Ot	servations		5			
50				of Freedom		3			
51	x,stds	258.8		-6.82168	!				
52			X Coeffic	ient(s)	0.235451				
53			Std Err o	f Coef	0.047382				

∢	<b>20</b>	ט	: ا	u	L.	9	<b>E</b>	_	7	<b>×</b>	<b>_</b>	Σ
BNL-FTA								,				
				:				i				i
:	1900	Samplemass	I MOIN			Measured		Dias%	Notes	Measured		Bias%
<u>a</u>	aCi/Sample g		n <b>B</b> q/g	nBq/Sam	Sigma1%	Sigma1% nBq/Sample	Sigma1%			nBq/g	Sigma1%	
- ! !	6 BLK	225	0	0		200				က	-	_
	8 BLK	216.5	0	0		1700	17.6			<b>∞</b>		-
ý	62 BLK	203.7	0	0		LOST	! !		Lost	Lost		!
œ́	83 BLK	199.6	!	0		*<700			Q I D	<3.5		
<b>5</b>	SE BLK	231.4		0		*<700			√ΓD	<3.0		
Avg/1sm						1200	57.83517			5.5	59 38157	
sm(nBq/unit)	<b>3</b>										-	
: !	100	! ! !	18.5114	4053.997	0.5	•<700			41D	<3.2	i	
	100		18.5114	4176.172	0.5		12	40 14		11	12	40 58
4	100	234	18.5114	4331.668	0.5	[			mislabled?	78		
9		· ·	18	3996.611	0.5			<b>↓</b>		14	- o	1
63	3 100	227.6	18.5114	4213.195	0.5		12.1			13	-	-29 77
Avg/1sm					0.5	2833.3	5.39	4		12.66867	6.028	++
31		:	46.2934	10076.22	0.5	11400	2.6	13.14		52		12.33
40			46.2934	10263.25	0.5	10000		-2.565		45	3.5	1.
53			46.2934	10247.04	0.5	0069				31		_
59	9 250	227.35	46.2934	10524.8	0.5	!				27		+-
9			46.2934	10367.41	0.5	3200				14	14	<del></del>
Avg/1sm					0.5	 	19.3	-26.65		33.8	19.87	-26.99
15	800	1	148.368	32715.14	0.5	*<700			C   C   C   C   C   C   C   C   C   C	<3.2		
20		209.4	148.368	31068.26	0.5	23200	1.5	-25.33		100	1.5	-326
20	800		148.368	31572.71	0.5	2600	+	-91.77	mislabled?	12	-	
2			148.368	31735.92	0.5	9100	3.3	-71.33		42		
ď	800	211.85	148.368	31431.76	0.5	34100	1.2			161	12	+
Avg/1sm					0.5	22133.3333	28.31496	-29.39		101	29.45857	
12			277.747	61159.89	0.5	27100	1.3	-55.69		123	13	-55 72
ဗ္ဗ	3 1500		277.747	57243.66	0.5	LOST			Lost	Lost		
42			277.747	57521.4	0.5	57000	0.0	-0.906		275	0	-0 989
73		206.7	277.747	57410.3	0.5			1		237		+
93			277.747	57688.05	0.5		6.2		trackoverlap *104			+
Ava/1c								• • • • • • •				

В	S	T	U	V	W	X	Y	Z	AA
3	NOSM	Meas							
4		nBq/g							
5		3							
6		8							
7		lost		-					
8		<5.5	<b>-</b>						
9		<5.5							
10	x,stds,del9	5.5	64.28243						+
_11									-+
12									-+
13									
14		<del></del>	·	<u>.</u>					
15		<5.5		egression	Output:				+
16	-0.82		Constant			12.66667			·
17	. 0		Std Err of Y I	Est		0.408248	2 22 1221		<del>_</del>
18	0.82		R Squared				0.981981	>0.879	Pass
19		78	No. of Obser			3			·
20		40.0000	Degrees of F		<del></del>	1	<del>-</del>		·
21	x,stds	12.66667	1.527525 -3	<del></del>	4 000000				+
22			X Coefficient		1.829268	<del></del>	<del>-</del>		
23		_	Std Err of Co	et.	0.352043				
24	4 40								
25	-1.13	14		egressior	Output:	20.0	<del></del>		<del></del>
26	-0.49		Constant	F - 1		33.8			
27	0		Std Err of Y	∟St		2.567429	0.00007	- 0 070	
28	0.49		R Squared				0.988987	>0.879	Pass
29	1.13	52	No. of Obser			5			+
30 31		20.0	Degrees of F			3	<del></del>	<del></del>	<del></del>
32	x,stds	33.8	15.02332 -		-17.06				<del></del>
33	•		X Coefficient		1.473977				
34	•		Std En of Co	er.	1.4/39//	· · · · · · · · · · · · · · · · · · ·			
35		<3.2	·		Output:				<del></del>
36			Constant	egressioi	i Output.	101			
37	-0.82		Std Err of Y	Ec+		1.224745			•
38	-0.02		R Squared	LSI			0.999894	>0.879	Pass
39	0.82		No. of Obser	vations		3	0.333034	- 0.070	1 000
40	0.02		Degrees of F			1			
41	x,stds	101		10000111					<del></del>
42			X Coefficien	t(s)	72.56098				:
43			Std Err of Co		1.056129				
44	-					······································			
45		104	R	egression	Output:				
46	-0.82		Constant			211.6667			
47	0		Std Err of Y	Est		31.02687			
48	0.82		R Squared				0.960769	>0.879	Pass
49		lost	No. of Obse	rvations		3			
50			Degrees of F	reedom		1			
51	x,stds	211.6667	<del>+</del>						
52			X Coefficien	t(s)	92.68293			•	
53			Std Err of Co	oef.	26.75526				

Target S	ampleMass	Known nBa/a	nRo/Sample Sigma1%	Signa 1%	Measured PRO/Sample	Sigmo19,	Bias%	Notes	Measured		Bias%
	201	00		2 3 3	• •			!-</td <td>&lt;-8.84 145</td> <td>249.1 31.6</td> <td></td>	<-8.84 145	249.1 31.6	
	208.8	0			-2310				-11.1	ļ	
	205.95	0	0		11500	39			99		
	209	0			-1490	294.4	:		-7.14	29	
	-				0006	79.65307			45.69	79.	
						7168.776				36.49759	
8	219.7	18.5114		0.5	6450	70.2	58.6		29.3	70.2	58.28
9	222.3	18.5114	·	0.5	8830	58.4	114.6		39.7	!	114.5
음 은	216.1	18.5114	-		0069	66.7	72.49		31.9	66.7	72.33
9	218.4	18.5114		0.5	7830	59.5	93.67		35.9	59.5	93.93
<u>8</u>	223.8	18.5114	4142.85132		:	78.2	68.72		31.3	78.2	69.08
				0.5	7400	5.693665	81.61	:	33.62	5.531462	81.62
250	224.7	46.2934	10402.127	0.5	19000	35.5	82.65		84.4	35.5	82.32
250	218.4	46.2934	10110.4786	0.5	15500	32.9	53.31		71.2	32	53.8
250	222.1	46.2934	10281.7641	0.5	17600	28.5	71.18		79.4		71.51
250	203.95	46.2934		0.5	<16800			۲. درل	<82.6		
250	217.6	46.2934	10073.4438	0.5	:	37.2	27.07		59	37.2	27.45
				0.5	16225	8.316212	58.55		73.5	7.546218	58.77
800	214.1	148.368	က	0.5	47700		50.16		223	12.2	50.3
800	216.75	148.368	32158.764	0.5	27800	17.6	-13.55		128	i i —	-13.73
800	211.3	148.368		0.5	23100		-26.32		109	ļ '	-26.53
800	205.85	148.368			36200		18.53	- 	176	17.1	18.62
800	220.1	148.368	32655.7968	0.5	22300	22.5	-31.71		5	22.5	-31.93
	+			0.5	31420	15.1	-0.578		147.4	15.57221	-0.652
1500	224.1	277.747	62243.1027	0.5	74000	8.2	18.89		330	8.2	18 81
1500	216.4	277.747	60104.4508	0.5	<74500			ς ΓΓ	<344		
1500	214.1	277.747	59465.6327	0.5	54400	8.7	-8.519	ļi ļ	254	87	-8.55
1500	218.1	277.747	60576.6207	0.5	20400	18			93.6	18	-66.3
1500	221.7	277.747	61576.5099			-			492		77.14
		:		0.5	64450	28.74043	5.265		292	28 3139	5.276

Α	<u> </u>	T	U	V	W	X	Υ	Z	AA
3	NOSM	Meas						•	
4		nBq/g							
5		<-8.84		Regressio	n Output:				
6	-1		Constant	·		45.69			
7	-0.29	•	Std Err of			31.26699			
8	0.29		R Squared		<del></del>	0.877681	0.936847	>0.868	Pass
9	1	145	<del></del>	servations		4		· +	
10	<del></del>	·		f Freedom	<u>.                                    </u>	2			
11	x,stds	45.69							
12	<del></del>		X Coeffici	ent(s)	80.44027			,	
13			Std Err of	Coef.	21.23422			<u> </u>	
14		00.0		·	<u> </u>	······································			
15	-1.13			Regressio	n Output:			<u> </u>	<del></del> -
16	-0.49		Constant			33.62			_ <del>-</del>
17	. 0		Std Err of			1.226299			
18	0.49		R Squared	3	<del> </del>		0.966838	>0.879	Pass
19	1.13	39.7	No. of Ob			5			-
20				f Freedom		3	·		
21	x,stds	33.62		81.61781					
22	•		X Coeffici		4.616348				
23		•	Std Err of	Coet.	0.704026				
24 25		400 C			- 0.1.				
	·	<82.6	0	Regressio	n Output:	70.5			+
26	-1		Constant			73.5			
27	-0.29		Std Err of			2.576897			
28 29	0.29		R Squared				0.981847	>0.868	Pass
30	1	04.4		servations		4			-
<u>30</u> 31	v otdo	73.5	Degrees o	f Freedom		2			
32	x,stds_	13.5	V 045-:		40.04455				<del></del>
33		•	X Coeffici		12.81155				
34		·	Std Err of	Coer.	1.750038			-	
3 <del>4</del> 35	1 12	101	• • • • • • • • • • • • • • • • • • • •	Dannai	- 0.44				
36	-1.13 -0.49			Regression	n Output:	4474		<u> </u>	
36 37	-0.49	<del></del>	Constant	V E-4		147.4			
37 38	0.49		Std Err of R Squared			17.64786	0.05.4630	> 0 070	
39	1.13		No. of Ob				0.954636	<i>&gt;</i> ∪.8/9	Pass
<del>39</del> 40	1.13			of Freedom		<u>5</u>	<del></del> ;		
<del>40</del> 41	x,stds	1A7 A		-0.65243					
42	^,3(U3	147.4	X Coeffici		56.25906		-		-
43			Std Err of		10.13174				
<del>43</del> 44			JIG ETT OF	CUEI.	10.13174	· · · · · · · · · · · · · · · · · · ·		<del></del>	·
45	- <del></del>	<344	· · · · · · · · · · · · · · · · · · ·	<del></del>	-	··· .			
<del>46</del>	-1	•	<del> </del>	Regressio	n Output:				<del></del>
47	-0.29		Constant		ii Output.	292.4			•
48	0.29	<del></del>	Std Err of			18.99419			
<del>40</del>	1	•	R Squared		· · · · · · · · · · · · · · · · · · ·		0.005604	>0 969	Door
<del>50</del>		432		servations			0.995604	<b>~</b> ∪.005	Pass
51	v etde	222.02		of Freedom		4		<del></del>	
52	x,stds	233.82	Deglees C	n rieedom	<u> </u>	2		•	·
53			V Cooffici	ont(c)	102.040			•	
54		•	X Coeffici		193.912				
J-4			Std Err of	Coel.	12.89945				



	⋖	∞	ပ	۵	Ш	L	O	I	_	7	¥	_	Σ
	PNNL												
			:										
	: : : : : : : : : : : : : : : : : : : :			Known					Bias%	Notes	Measured		Bias%
	۵	Sample	O1	nBq/g	nBq/Sample	Sigma1%	nBq/Sample	Sigma1%			nBq/g	Sigma1%	
:	2	R.K	205.4		0					:	170		
	7	8LK	225.5	0	0		*100000	80		Low CY	•500		<u> </u>
	10	10 BLK	206.1		0	i i	<10000		! !	ςFD	<50		
:	38	38 BLK	212.45		0		<20000				×100		1
:	9/	BLK	221.85	0	0	; ;	23000	59		}	5	5.0	
	Ava/1sm						28500	19 208			125	25 025	
-	sm/nRn/unit)		1				2002		1		3	-	
+	24	100	219.8	18 5114	4068 R0572	0.5	21000		416.1		2	400000	407.0
	42		222 5	ď	·-		/2000		2	2	2	2	-
-	2		224 6	2		3 0				יייי יייייייייייייייייייייייייייייייי	001	7	
	0 4		2000	-   •	-	2 0	3			) MOI	200		- i
	ρ		CR.077			ဂ ာ			(3		160		764.3
	69	100	230.3	18.5114	4263.17542	0.5		28	979		200	28	980.4
	Avg/1sm		1			0.5	34666.6667	21.08818	722.7		151.3333	20.42172	717.5
	17	250	214.7	46 2934	9939 1929R	2.0	*20000	62		>0	<b>*</b>	7	
*	30		213.2		9869 75288	0.5					250	2	
	34		213.5	: _		0.5			i	) - - -	4100		
	49		223.5	!	-	0.5		8	586.2		320	3	591 2
	2	250	220.1	46.2934	10189.1773	0.5	25000		145.4		120		159
	Avg/1sm					0.5		47.916	365.8		220	45.454	<u> </u>
			1										1
٠	4	800	214.65	148.368	31847.1912	0.5	48000	30	50.72		230	30	55.02
	23		216.25	. !	32084.58	0.5	23000	67	-28.31		110		
	28	800	212.3	148.368	31498.5264	0.5	120000	46	281		550		
	72	8	213.9	148.368	31735.9152	0.5	28000	112	-11.77		130	-	
	<b>7</b> 6	800	216.5	148.368	32121.672	0.5	78000	47	142.8		380	47	142.6
	Avg/1sm				,	0.5	59400	30.25436	86.89		276	29.55953	86.02
-													
	က	1500	208.5		57910.2495	0.5	67000	49	15.7		320	49	15.21
÷	\$	,	209	1	58049.123	0.5	_	27	89.49		510	27	83.62
<b>-</b>	88		213.2		59215.6604	0.5	73000	30	23.28		350		26.01
	97	1500	212.75	277	59090.6743	0.5	110000	35	86.15		200	35	80.02
	66		207.9	277.747	57743.6013	0.5	80000	31	38.54		380	31	40.42
	A.145.00	-				4	ססטאא	10 47059	50 B2		7+7	1070700	90

D	S	T	U	V	W	X	Y	Z	AA
3	NOSM	Meas			I				
4		nBq/g	1		!	·		1	
5		170			·	Ţ <del>.</del>	<del> </del>	†	
6		*500				†		+	
7		<50		1	†	*	··	•	
8		<100	1	<del>                                     </del>	<u> </u>	<u> </u>	<u> </u>	+	+
9		100		<del></del>	·	<del> </del>	<del>                                     </del>	†	
	x,stds	135	<del>+</del>		<u>†</u>	<del> </del>	<del> </del>	<del> </del>	
11	A,5tG5	100	50.0040	<u> </u>	<u>+</u>		•	<del>†</del>	
12			<del></del>		<del></del>	†	<del></del>	+	
13		<del></del>		<del></del>		<del> </del>	<del></del>	<del> </del>	
14		<u> </u>	+	<del> </del>		<u> </u>		<del></del>	·- <del>-</del>
15		*20	<del> </del>	Di-	- 0.4- 4.	•			
		*30	-	Regressio	n Output:		+	<u> </u>	<u> </u>
6		<100	Constant	<del></del>	<u>:</u>	151.3333	ļ	ļ	
17	-0.82		Std Err of		n Output:	10.61446			·
8	0		R Squared			0.98034	0.990121	>0.879	Pass
9	0.82	200	No. of Obs			. 3			
20				f Freedom		1			
21	x,stds	151.3333	35.37146				i		1
22			X Coefficie	ent(s)	64.63415	1			
23			Std Err of	Coef.	9.153114	+		<del> </del>	
24								!	
5		*90	,			!			•
26		<50		···	<del></del>			<del></del>	
27		<100				+			· · · · · · · ·
8		320			<del></del>	-		<del>i-</del>	
9		120		·	<del></del>				
10		120							· - i
	v otelo	220	64 20242			<del> </del>			<del></del>
	x,stds	220	64.28243			<del> </del>		-	
2									
3									<u> </u>
4			 		·	·			
5	1.13	110		Regressio	n Output:	—		L	
6	-0.49		Constant			276			
7	0		Std Err of			59.2082			
8	0.49	360	R Squared			0.920997	0.959686	>0.879	Pass
9	1.13		No. of Obs			5			- <del>+</del>
0			Degrees o			3			
1	x,stds	276	66.09713						
2			X Coefficie	ent(s)	201.0218				
3		+	Std Err of		33.99179				
4				= = = = = = = = = = = = = = = = = = = =					<del> </del>
5	-1.13	320	•	Regression	n Output:				
6	-0.49		Constant	. 1091000101	· Output.	414			
7	0.49		Std Err of	V Est					
.8					······	30.24263	0.050004	- 0 0 70	
	0.49		R Squared				0.953364	>U.8/9	Pass
9	1.13	510	No. of Obs			5			<b></b>
0			Degrees of	r ⊢reedom		3			
	x,stds	414	20.96028		·- <del></del>				<del></del>
2			X Coefficie		94.99011				. +
3	I		Std Err of	Cnef	17.36248		1		

	<	۵	>	2	u	<b>L</b>	פ	E	_
	mda								
=	lab	NIST	Reported	Random	Systemmatic Random	Random	Systemmatic	mda	mda
-		nBq/g	nBq/g	sm1%	sigma1%	sm1(nBq/g)	sm1(nBq/g) sigma1(nBq/g nBq/g	nBq/g	at "0" nBq/g
<u> </u>	BNL ICP-MS	BLANK	-0.025	5931.55	10.7	1.4828875	0.002675	9.242649	7.9
$\vdash$		18.5	14.8	6.416846	10.7	0.9496932	1.5836	6.993474	CL95% = 22%
		46.3	40.5	2.589651	10.7	1.0488087	4.3335	7.40138	
		148.4	136	0.600365	10.7	0.8164964	14.552	6.452636	
		277.7	259	0.603574	10.7	1.5632567	27.713	9.593352	
-									
_	BNL FTA	BLANK	5.5	59.38157	18.9	3.2659864	1.0395	21.13697	9
-		18.5	12.7	6.029705	18.9	0.7657725	2.4003	6.826113	CL95% = 1900%
<del> </del>		46.3		19.87761	18.9	6.7186322	6.3882	50.13683	
		148.4	101	29.45857	18.9	29.753156	19.089	517.8243	
		277.7	212	21.57653	18.9	45.742244	40.068	1122.893	
_	LANL TIMS	BLANK	45.7	79.88091	0.287	36.505576	0.131159	131.1281	3
		18.5	33.6	5.531462	0.287	1.8585712	0.096432	9.160743	CL95% = 585%
-		46.3	73.5	7.546218	0.287	5.5464702	0.210945	0.210945 21.48596	
		148.4	147	15.57221	0.287	22.891149	0.42189	81.55305	
-		277.7	767	28.3139	0.287	82.676588	0.83804	315.1431	
=	PNNL ICP-M	BLANK	135	25.92593	22.4	35.000006	30.24	816.347	455
		18.5	151	20.42172	22.4	30.836797	33.824	649.2829	CL95% = 3600%
		46.3	220	45.45455	22.4	100.0001	49.28	5889.889	
$\vdash$		148.4	276	29.55953	22.4	81.584303	61.824	3982.039	
-		277.7	414	9.373724	22.4	38.807217	92.736	985.7653	

Table 4

l able 4				
Uncertainty	BNL ICP-MS	BNL FTA	LANL TIMS	PNNL ICP-MS
Replicate & Random	(1s <sub>m</sub> , %)	(1s <sub>m</sub> , %)	(1s <sub>m</sub> , %)	(1s <sub>m</sub> , %)
Concentration (nBq/g) Blank	5900	29	80	26
18.5	6.4	0.9	5.5	20
46.3	2.6	20	7.5	45
148.4	09.0	29	16	30
277.7	09.0	22	28	9.4
Tracer	5.8	5.8	0.25	10
Chemical Yield	თ	15	•	
Other	ı	10 (Thermal Flux)	0.1 (Geometry) 0.1 (Spectral Interference)	1 (Geometry) 20 (Spectral Interference)
Total Propagated Uncertainty				
Concentration (nBq/g) Blank	2900	62	80	34
18.5 46.3	7 7	20 27	5.5 7.6	30 51
148.4		35	16 28	37
1.112	-			

## **Outlier Tests**

Because the primary objective of this intercomparison is to evaluate the mass spectrometric technology for its ability to measure plutonium (239) in synthetic urine, the best reported data was to be used for the evaluation. Each laboratory was asked to review their data carefully for accuracy, and to note data that of poor confidence. Those data that were noted as unreliable were reported but not used in this evaluation. The remaining data were evaluated for normal distribution. Filliben's r criteria for goodness of fit of normal probability plots was used to detect outlying data (J.J. Filliben, The Probability Plot Correlation Coefficient Test for Normality, Technometrics, 17 (1), 111-117 (1975)). Outlier data were also not used in this evaluation. Included with the spreadsheets (1-4) are the assessment of the distribution of the reported nBq/g values. Normal probability plots of the data are displayed in Figures 1-17. The linearity of the data, r, is evaluated against the Filliben acceptance criteria. The spreadsheets include the following information:

NOSM

Meas (nBq/g)

x, stds

Regression Output

Normal Ordered Statistic Medians for each

reported concentration value

Reported concentration value

Mean and percent standard deviation of

reported concentration values

R squared is the goodness of the regression fit, followed by R, Filliben's acceptance criteria, and decision that the data is not statistically different from a normal distribution when R >

Filliben's criteria

### Technical Issues

The results of this study can now be used to address the technical issues raised during the design of the study protocol.

- o Stability of the plutonium in glass bottles and in the synthetic urine: As a minimum, over the short-term of a few weeks and by washing the bottle with strong acid, the plutonium appears to be stable in the glass bottles and in the synthetic urine. BNL ICP-MS results indicate stability of the test samples to better than 8 percent at the 148-278 nBq/g levels, and better than 20 percent at the 15-41 nBq/g levels.
- O Contamination from plutonium in the reagents used to make the synthetic urine: The BNL ICP-MS and FTA results indicate contamination of the test samples by plutonium in chemical reagents to be negligible ( < 6 nB/g, and probably as low as ≈ 0.03 nBq/g).

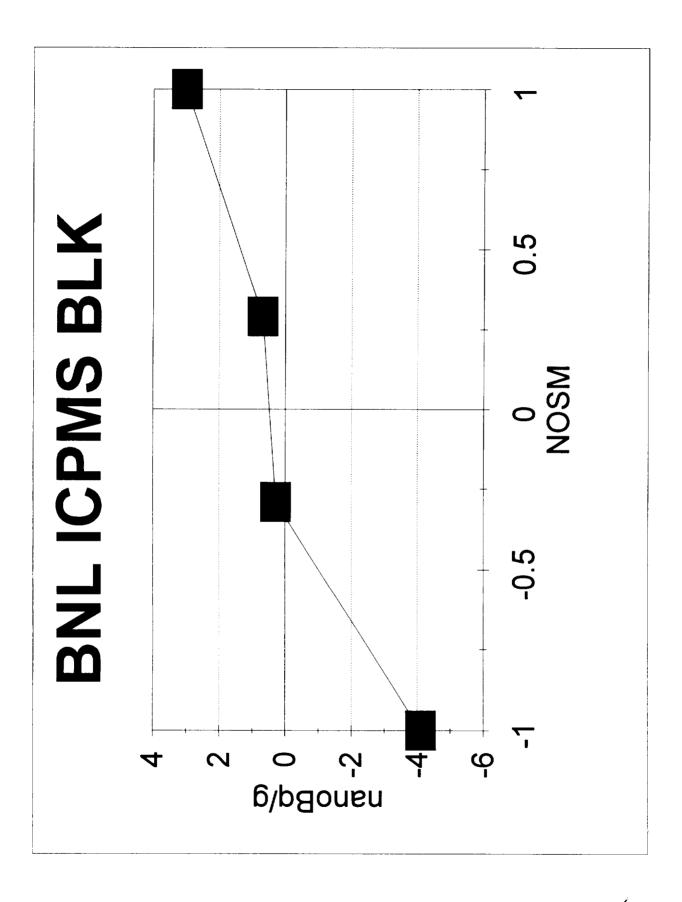
0 Adequacy of the synthetic urine as a substitute for natural urine: The ANSI N13.30 standard allows use of synthetic urine as a test matrix, synthetic urine was used for pilot testing the efficacy of the ANSI N13.30 standard, and synthetic urine will be used for the radiobioassay DOE Laboratory Accreditation Program. However, it was pointed out by all of the participating laboratories that chemical yields were substantially lower than anticipated. For example, LANL reported chemical yields as low as 20 percent - their average chemical yield for radiourine assay is 80 percent. The low chemical yield substantially lowers analytical sensitivity and increases measurement uncertainty. A systematic study will be necessary at each laboratory to optimize chemical yield from synthetic urine analysis. It is likely, however, that the resulting analytical protocol will be substantially different from that in daily use for natural urine. None the less, the results of this study provides a lower limit to mass spectrometry's capabilities, from which improvements can be built.

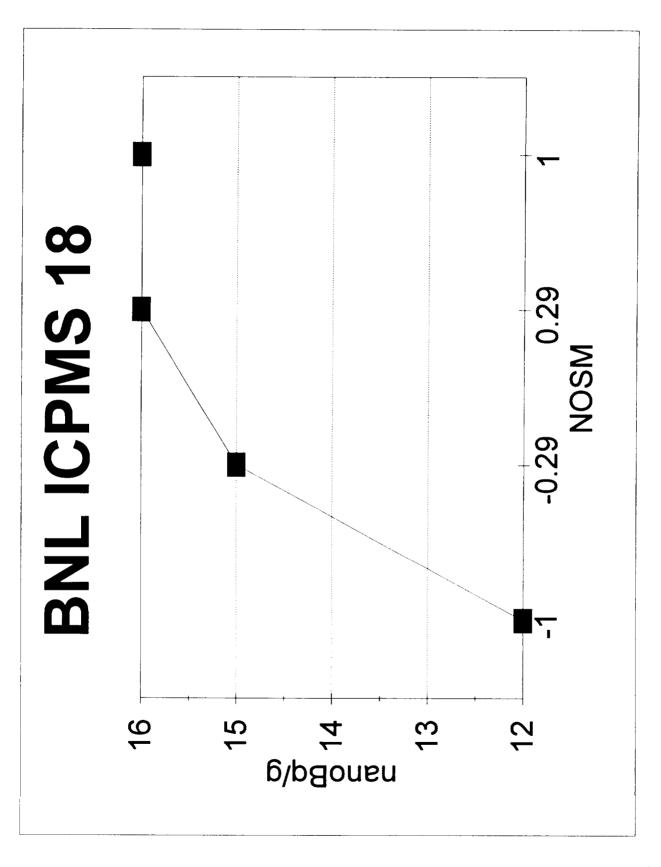
Figures 1-5

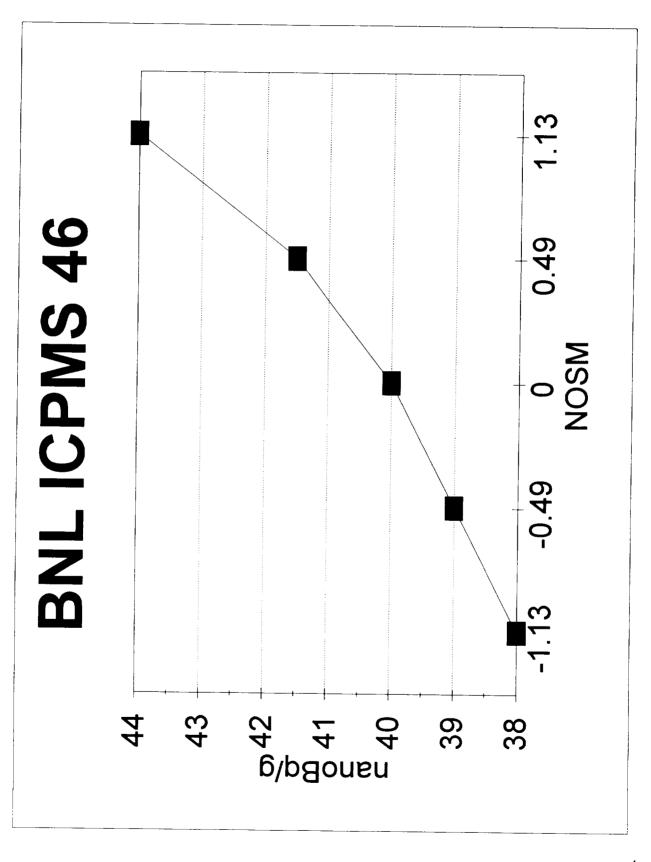
**BNL ICP-MS** 

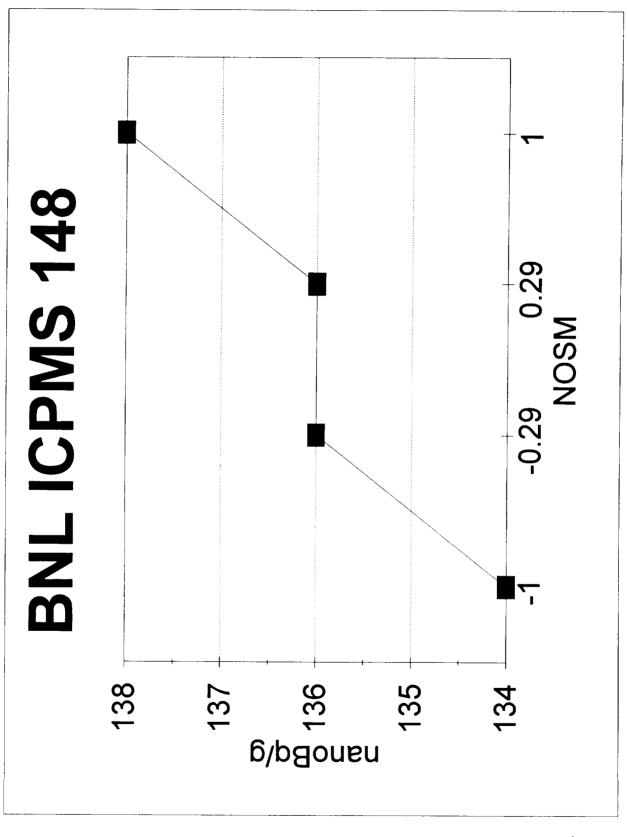
**NOSM** 

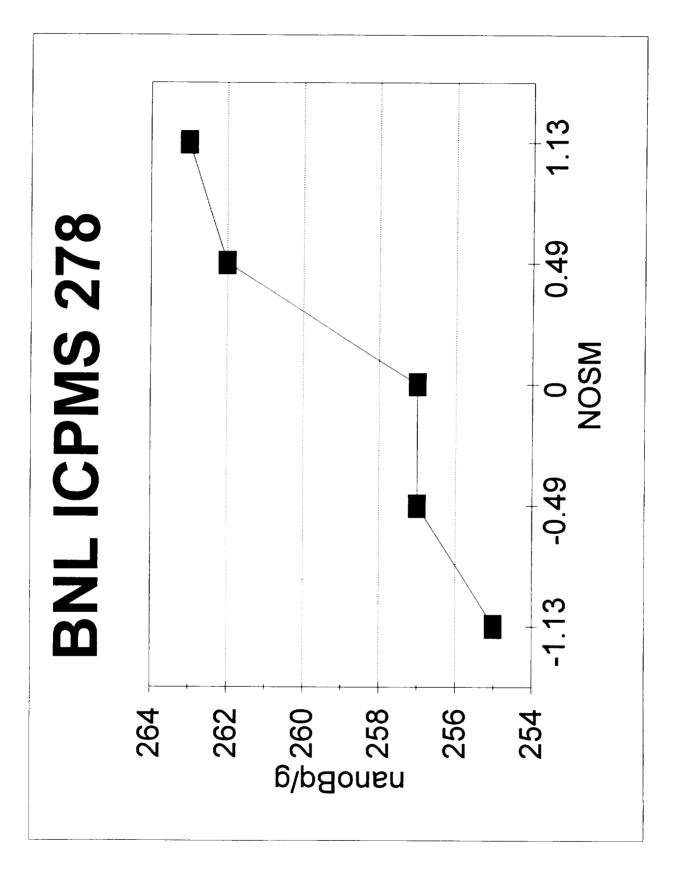
Fn:kinn/yael/puurine.pap/September 11, 1997







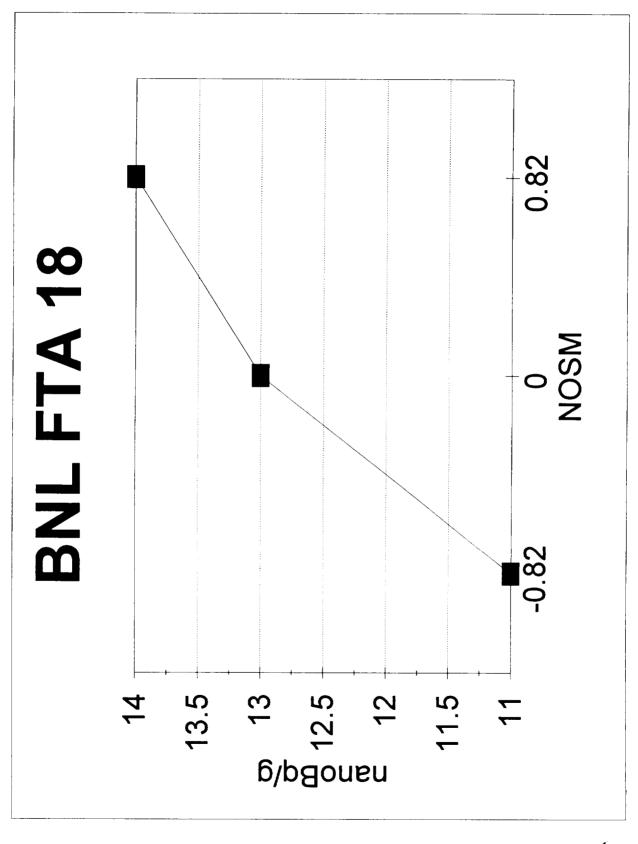


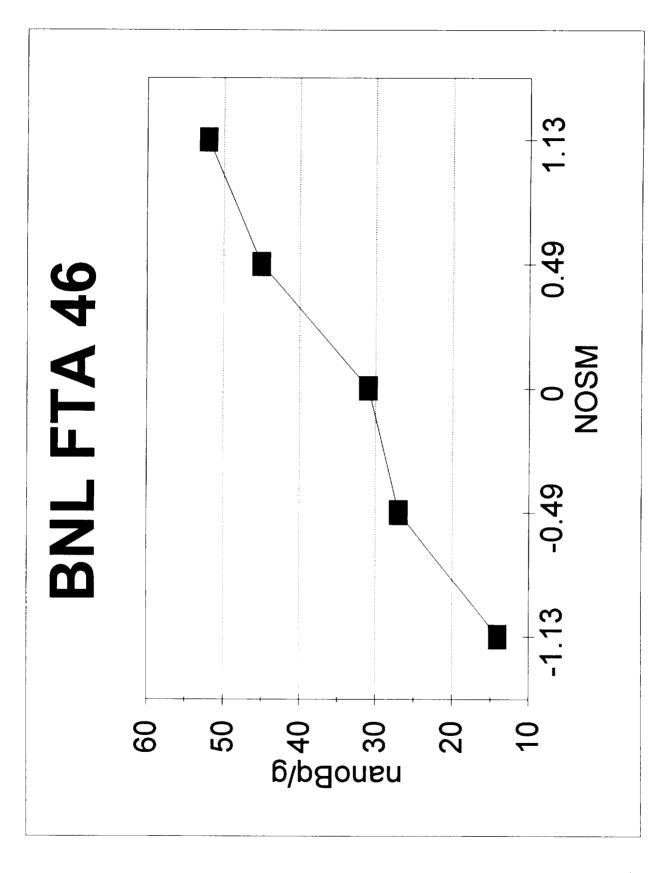


Figures 6-9

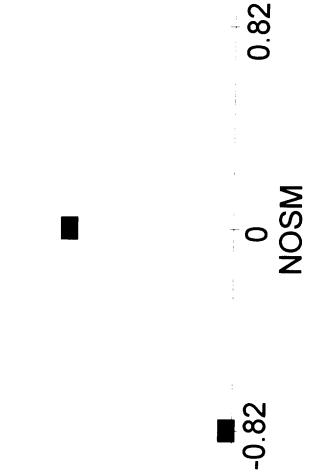
**BNL FTA** 

**NOSM** 





## **BNL FTA 148**



## **BNL FTA 278**

NOSM

0.82

**■**-0.82

280 260 240 220 180 140 120

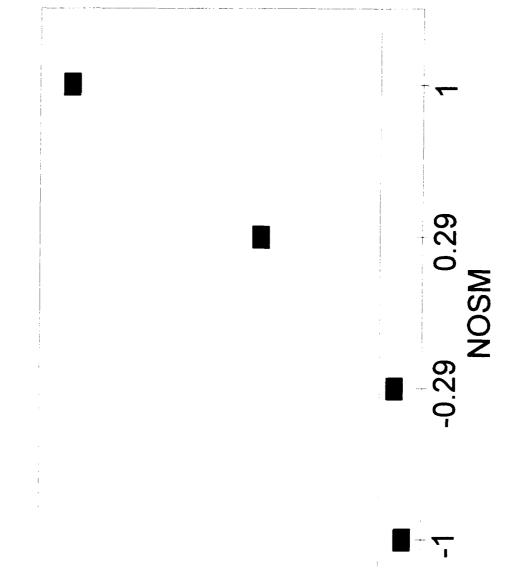
Figures 10-14

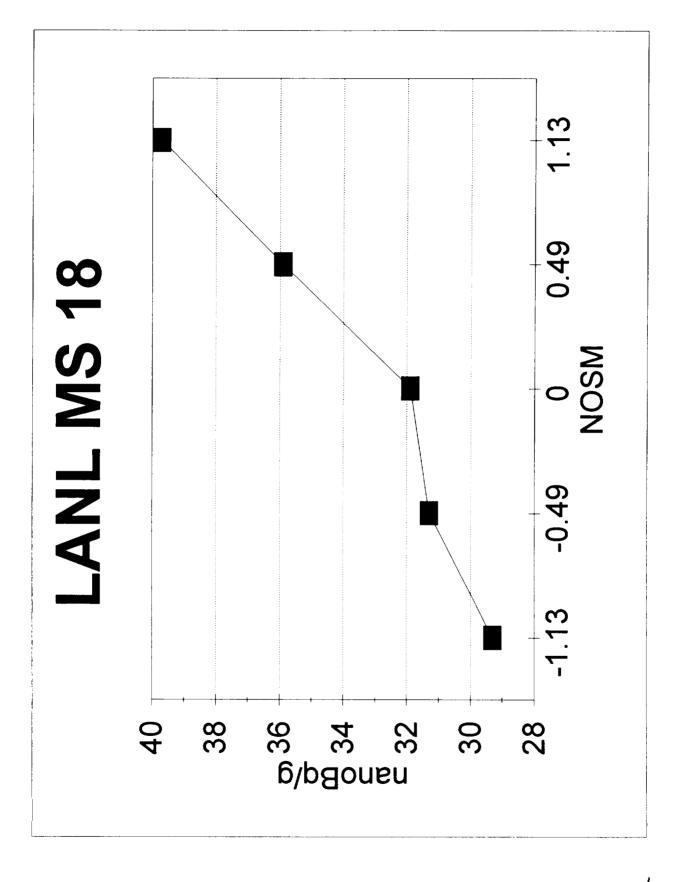
LANL TIMS

**NOSM** 

Fn:kinn/yael/puurine.pap/September 11, 1997

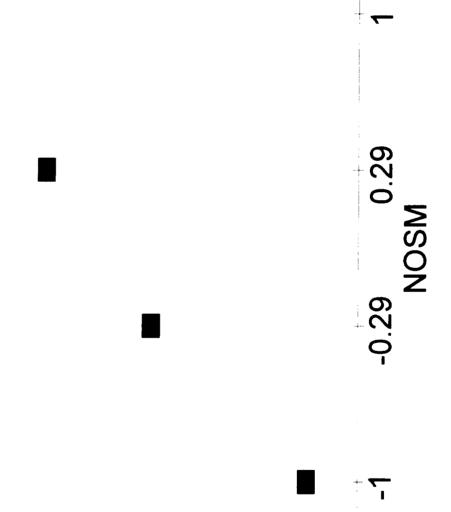
# -ANL MS BLK







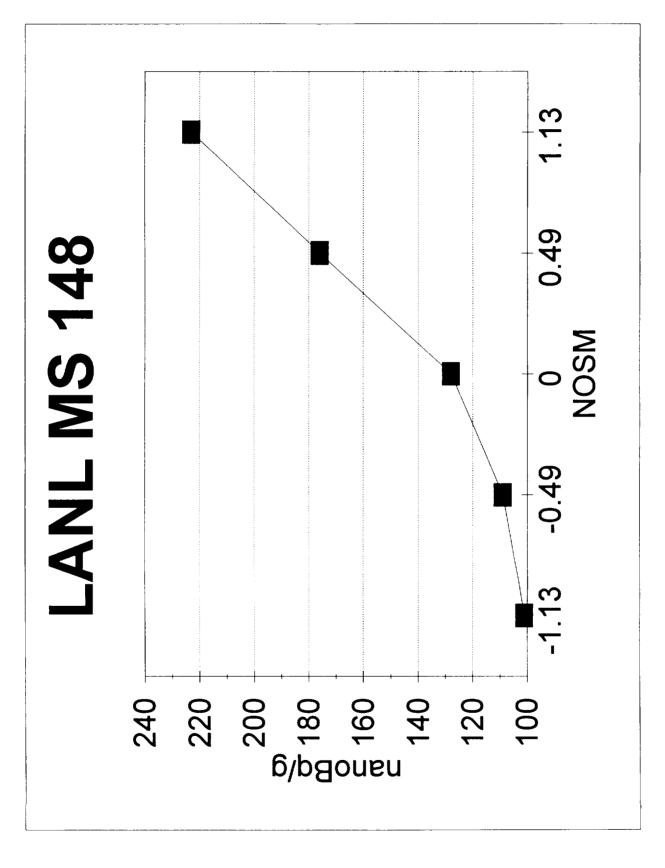
## LANL MS 46



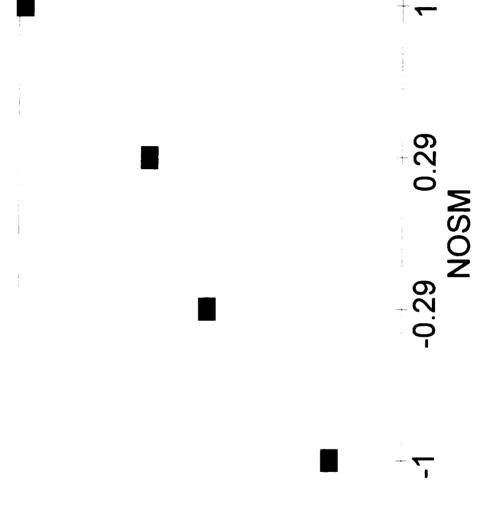
nanoBq/g 65 65

9

80



# LANL MS 278

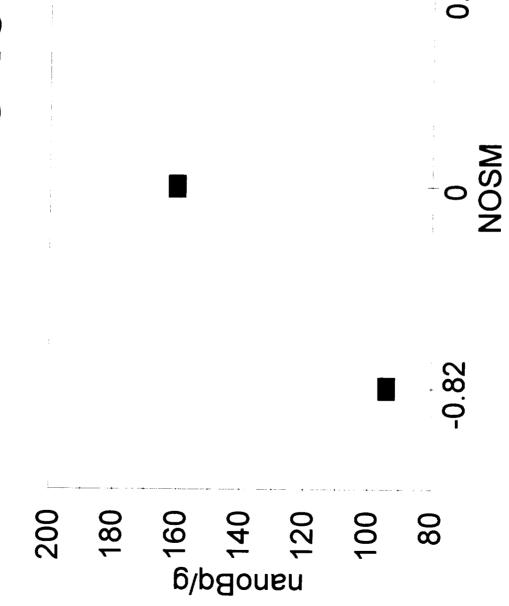


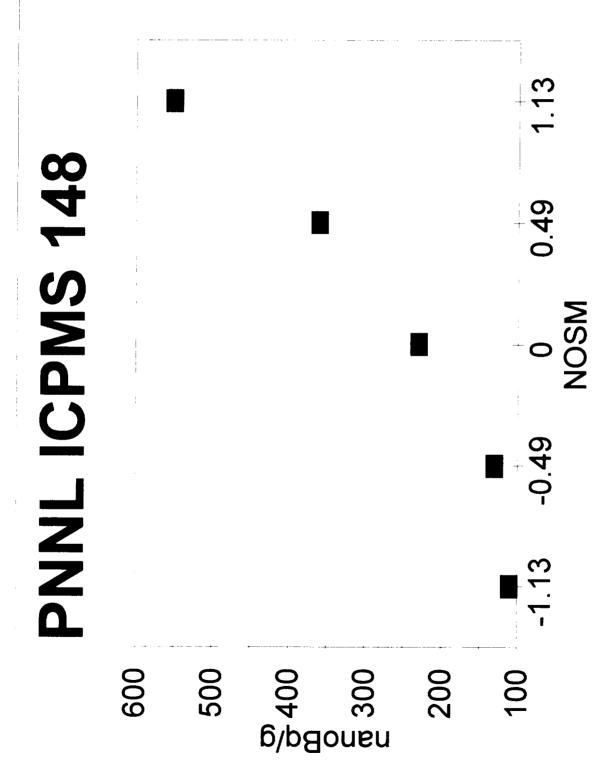
nanoBq/g

Figures 15-17

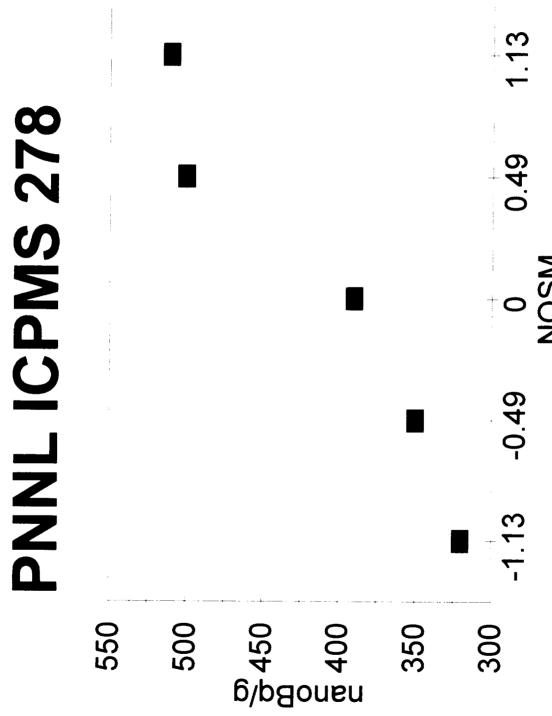
PNNL ICP-MS
NOSM

# PNNL ICPMS 18









### VI. REPORT of TRACEABILITY

### U.S. Department of Commerce National Institute of Standards and Technology Gaithersburg, MD

### REPORT OF TRACEABILITY

### **PLUTONIUM-239**

### U.S. Department of Energy International Health Programs, EH-63 Germantown, MD, USA

Test Identification

DOE/EH63/97

Matrix Description

<sup>239</sup>Pu in synthetic urine solution

Source Description

Solution in glass bottle<sup>1</sup>

Test Concentrations

18.5, 46.3, 148, and 278 nBq•g<sup>-1</sup>

Reference Time

12:00 noon, February 26, 1997

### **RESULTS:**

Per ANSI N42.22 criteria for traceability testing, the results indicate measurements of <sup>239</sup>Pu at the testing concentrations were acceptable at the stated uncertainties by:

- a) Brookhaven National Laboratory Inductively Coupled Plasma Mass Spectrometry for the 18, 46, 148 and 278 nBq/g levels;
- b) Brookhaven National Laboratory Fission Track Analysis for the 18, 46, 148, and 278 nBq/g levels;
- c) Los Alamos National Laboratory Thermal Ionization Mass Spectrometry for the 148 and 278 nBq/g levels; and
- d) Pacific Northwest National Laboratory Inductively Coupled Plasma Mass Spectrometry for the 148 and 278 nBq/g levels.

Per ANSI N13.30 criteria for bias and precision testing, the results indicate measurements of <sup>239</sup>Pu at the testing concentrations were acceptable for both criteria by:

- a) Brookhaven National Laboratory Inductively Coupled Plasma Mass Spectrometry for the 18, 46, 148 and 278 nBq/g levels;
- b) Brookhaven National Laboratory Fission Track Analysis for the 278 nBq/g level;
- c) Los Alamos National Laboratory Thermal Ionization Mass Spectrometry for the 148 and 278 nBq/g levels; and
- d) Pacific Northwest National Laboratory Inductively Coupled Plasma Mass Spectrometry for the 278 nBq/g level.

Samples distributed Report received

February 28, 1997 May 30, 1997 For the Director

J. M. R. Hutchinson Group Leader Radioactivity Group Physics Laboratory

gu Mattetin

## TEST RESULTS

Nuclide	Z	NIST Values	Rep Brookl L	Reported Value <sup>6</sup> Brookhaven National Laboratory	Difference	ANSI N42.22 Traceable	ANSI N42.22 Traceability Limit <sup>7</sup>	ANS C <sub>I</sub>	ANSI N13.30 Criteria (Pass/Fail)*
Sample Number	nBq per gram²	Relative Expanded Uncertainty <sup>3,4,5</sup> (2s <sub>m</sub> percent)	nBq per gram	Reported Uncertainty (2s <sub>m</sub> , percent)	(Percent)		(Percent)	Bias	Precision
PUR100	18.5	1.0	14.7	25	-20	Yes	±37	Pass	Pass
PUR250	46.3	1.0	40.5	22	-13	Yes	+33	Pass	Pass
PUR800	148	1.0	136	21	-8.3	Yes	+32	Pass	Pass
PUR1500	278	1.0	259	21	-6.8	Yes	± 32	Pass	Pass
BLANK	0	•	0.025	12000	ı	•	•	•	•

"0.1 $\pi$ " a defined-solid-angle counter with scintillation detector, $4\pi\alpha$ liquid scintillation and high purity germanium counting systems	NIST	BROOKHAVEN NATIONAL LABORATORY
	counter with scintillation detector, 4πα liquid the purity germanium counting systems	iductively Coupled Plasma Mass Spectrometry

Nuclide	Z	NIST Values	Report Brookh	Reported Value <sup>6</sup> Brookhaven National Laboratory	Difference	ANSI N42.22 Traceable	ANSI N42.22 Traceability Limit <sup>7</sup>	ANSI Cr (Pas	ANSI N13.30 Criteria (Pass/Fail)
Sample Number 23 <b>9Pu</b>	nBq per gram²	Relative Expanded Uncertainty <sup>3,4,5</sup> (2s <sub>m</sub> , percent)	nBq per gram	Reported Uncertainty (2s <sub>m</sub> , percent)	(Percent)		(Percent)	Bias	Precision
PUR100	18.5	1.0	12.7	40	-32	Yes	09 ∓	Fail	Pass
PUR250	46.3	1.0	33.8	55	-27	Yes	± 82	Fail	Pass
PUR800	148	1.0	101	70	-32	Yes	± 105	Fail	Pass
PUR1500	278	1.0	212	57	-24	Yes	98 <del> +</del>	Pass	Pass
BLANK	0	ı	5.5	125	•	•	•	1	

BROOKHAVEN NATIONAL LABORATORY	Fission Track Analysis
NIST	"0.1 $\pi$ " $\alpha$ defined-solid-angle counter with scintillation detector, $4\pi\alpha$ liquid scintillation and high purity germanium counting systems

Reported Value <sup>6</sup> Los Alamos National Laboratory	Difference	ANSI N42.22 Traceable	ANSI N42.22 Traceability Limit'	ANSI Cri (Pasi	ANSI N13.30 Criteria (Pass/Fail)
nBq Reported per Uncertainty gram (2s <sub>m</sub> , percent)	Reported (Percent) Uncertainty 2s <sub>m</sub> , percent)		(Percent)	Bias	Precision
34 11	1 82	No	+17	Fail	Pass
74 15	5 59	No	± 23	Fail	Pass
147 31	-0.7	Yes	+ 47	Pass	Pass
292 57	5.3	Yes	+ 85	Pass	Pass
46 160	<u> </u>	,	•	1	1

LOS ALAMOS NATIONAL LABORATORY	Thermal Ionization Mass Spectrometry
NIST	"0.1 $\pi$ " $\alpha$ defined-solid-angle counter with scintillation detector, $4\pi\alpha$ liquid scintillation and high purity germanium counting systems

Nuclide	Z	NIST Values	Rep Bai North	Reported Value <sup>6</sup> Battelle-Pacific Northwest National Laboratory	Difference	ANSI N42.22 Traceable	ANSI 42.22 Traceability Limit <sup>7</sup>	ANSI Cr (Pas	ANSI N13.30 Criteria (Pass/Fail)
Sample Number 239Pu	nBq per gram²	Relative Expanded Uncertainty <sup>3,4,5</sup> (2s <sub>m</sub> , percent)	nBq per gram	Reported Uncertainty (2s <sub>m</sub> , percent)	(Percent)		(Percent)	Bias	Precision
PUR100	18.5	1.0	151	61	718	No	± 91	Fail	Pass
PUR250	46.3	1.0	220	101	375	No	± 152	Fail	Fail
PUR800	148	1.0	276	74	98	Yes	± 111	Fail	Pass
PUR1500	278	1.0	414	49	49	Yes	± 72	Pass	Pass
BLANK	0	ı	135	69	•	1	•	t	٠

NIST	BATTELLE-PACIFIC NORTHWEST NATIONAL LABORATORY
"0.1 $\pi$ " $\alpha$ defined-solid-angle counter with scintillation detector, $4\pi\alpha$ liquid scintillation and high purity germanium counting systems	Inductively Coupled Plasma Mass Spectrometry

### **Notes**

(1) Five test-sample bottles for each concentration were provided for this test. Each sample consisted of approximately 200 g synthetic urine solution contained in a sealed glass bottle.

Composition of the Synthetic Urine

Component	<u>a/ka</u>
Urea	16.00
NaCl	2.32
KCI	3.43
Creatinine	1.10
Na₂SO₄ (anhydrous)	4.31
Hippuric Acid	0.63
NH <sub>4</sub> CI	1.06
Citric Acid	0.54
MgSO₄ (anhydrous)	0.46
NaH₂PO₄ ● H₂O	2.73
CaCl₂ ● 2H₂O	0.63
Oxalic Acid	0.02
Lactic Acid	0.094
Glucose	0.48
Na₂SiO₃ ● 9H₂O	0.071
Pepsin	0.029
Conc. Nitric Acid	50.00
Yellow Food Color (optional)	0.06

(2) Gravimetric dilutions of Standard Reference Materials were confirmed by replicate (n=5, at each concentration level) radioactivity measurements.

(3) The analysis methodology and nomenclature used for the reported uncertainties for NIST values are based on uniform guidelines [cf., B.N. Taylor and C. E. Kuyatt, NIST Technical Note 1297 (1994)] and are compatible with those adopted by the principal international metrology standardization bodies. Individual uncertainties have the significance of one standard deviation of the mean, or an approximation thereof. The relative combined uncertainty, u<sub>c</sub>, is the quadratic combination of the standard deviation (or standard deviation of the mean where appropriate), or approximation thereof, for the following component uncertainties:

### Source of Uncertainty

### Uncertainty

a) Gravimetric measurement

0.35 percent

b) <sup>239</sup>Pu certified uncertainties

0.36 percent

The individual certified uncertainties of standard reference materials are based on the quadratic combination of all sources of uncertainty manifest in the preparation the material. These uncertainties may result from uncertainties from any or all of the following: alpha-decay emission rate, background, balance calibration, decay corrections, decay-scheme data, extrapolation of alpha-particle-count-rate-versus-energy to zero energy, live time, alpha-particle detection efficiency, alpha-emitting impurities, gamma-emitting impurities.

The relative expanded uncertainty, U, is obtained by multiplying  $u_c$  by a coverage factor of k=2 and is assumed to provide an uncertainty interval of approximately 95 percent confidence.

(4) Impurities (SRM 4330A solution)

none detected

Estimated limits of detection for photon-emitting impurities are:

2.00 x 10<sup>-4</sup> γ ·s<sup>-1</sup> for energies between 42.5 and 90 keV,

8.0 x 10<sup>-5</sup> y •s<sup>-1</sup> for energies between 102 and 125 keV,

 $3.0 \times 10^{-6} \, \gamma \cdot s^{-1}$  for energies between 133 and 1456 keV,

8 x 10<sup>-6</sup> y •s<sup>-1</sup> for energies between 1465 and 3500 keV.

Provided that the photons are separated in energy by 4 keV or more from photons emitted in the decay of plutonium-239.

Alpha-emitting impurities (SRM solution)

none detected

Estimated limits of detection for alpha-particle-emitting impurities are:

0.04 α·s<sup>-1</sup> for energies less than 4.9 MeV and

0.001  $\alpha \cdot s^{-1}$  for energies greater than 5.2 MeV.

From mass-spectrometric measurements performed by the supplier, the massic activity ratios of other detected radionuclides (at 1200 EST, 4 December 1995) are:

(5) Half-life <sup>239</sup>Pu

- $24119 \pm 26 \text{ years}$
- (6) Test results were evaluated based upon reported measurements. Values from results associated with low chemical yield, below detection limits, and outlier test of normal distribution were not included in the evaluations.
- (7) ANSI N42.22 defines the traceability limit to NIST for performance testing as:

$$|V_N - V_L| \le 3 * \sqrt{(\delta_N^2 + \delta_L^2)}$$

Where:  $V_N = NIST Value$ ;

V<sub>L</sub> = Laboratory Value;

 $\delta_{N} = 1$  sigma total uncertainty of the NIST value,  $V_{N}$ ; and

 $\delta_L = 1$  sigma total uncertainty of the Laboratory value,  $V_L$ .

(8) ANSI N13.30 defines criteria for acceptable bias between -25 to +50 percent, and acceptable precision between -40 to +40 percent, 1 sigma total propagated uncertainty.

Information contacts: Dr. Kenneth G. W. Inn (301) 975-5541

### References:

ANSI National Standards Institute, ANSI N42.22-1995, "Traceability of Radioactive Sources to the National Institute of Standards and Technology (NIST) and Associated Instrument Quality Control."

ANSI National Standards Institute, ANSI N13.30-1996, "Performance Criteria for Radiobioassay."

### VI. ANALYTICAL ISSUES

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### **Analytical Problems**

Aside from misidentified samples and computation errors, this study revealed the following analytical problems:

Analytical Bias - Generally, biases approaching 5 percent are observed for the higher concentration test samples. It is likely that the accuracy of the chemical yield monitors (tracers) is a considerable portion of this bias. Careful preparation of yield monitors should remove most of the analytical bias. In addition, FTA is handicapped with a serious bias limitations when track density is high, and when batch chemical yield corrections are used. These sources of error severely limit FTA from being capable of being improved.

<u>Uncertainties</u> - BNL FTA, LANL TIMS and PNNL ICP-MS relative uncertainties increased with increasing plutonium concentration - This is contrary to intuition and should be investigated for root cause by each laboratory.

<u>Imprecision</u> - Most of the poor precision is caused by high variable blanks and low chemical yield (see below). Large measurement uncertainty could result in failing the ANSI N13.30 criteria for precision.

High Variable Blank - LANL and PNNL's results suffered from high and variable blanks. BNL ICP-MS results, by contrast, had very low and consistent blanks. Presumably, BNL has developed extreme sensitivity to sample and reagent contamination, and have developed extraordinary cleanroom techniques and ultra-pure reagents for analysis. The results of this study indicate that BNL's successes is strongly linked to their ability to control and minimize any blank contributions. LANL and PNNL should undertake careful study of their analytical system to seek out and control sources of contamination.

Low Chemical Yield - Discussions with the investigators indicated that chemical yields for natural urine samples are typically in the 70-80 percent range. The synthetic urine used in this study caused chemical yields to occasionally decrease to 20 percent. The root cause should investigated, particularly because it causes this technology evaluation to be inaccurate (particularly the evaluation of precision and MDA), and because the radiobioassay DOELAP effort will use the synthetic urine as the test matrix.

<u>Lost Data</u> - 21 percent of the reported results were not included in the study because of <MDA, analytical outlier, poor precision, overlapping tracks, or even poor reliability. This fraction is unacceptably high for production line operations. The reliability of the analytical systems must be improved through systematic

methods evaluations at each participating laboratory and brought under statistical control. Presumably, highly experienced analysts would be used to analyze the DOE-Marshall Islander urine samples because of the program's high political profile.

### **Study Limitation**

A serious limitation to this study is the absence of important isobaric and chemical interferences in the synthetic urine matrix. Addition of interferences would have also tested chemical separations and measurement selectivity. Interference that are present in natural urine include calcium, iron, lead, uranium and thorium isotopes, <sup>240</sup>Pu and <sup>241</sup>Pu. The results of this study should be interpreted as being collected under optimum conditions. Including interferences would have more closely simulate analytical performance on natural urine.

In spite of these study shortcomings, sufficient data exists to address the underlying objectives of this study, and will be provided in the next section.

### VII.

### **STATE-of-the-ART**

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### **Precision**

Total Propagated Uncertainties (K=3) are displayed in Figures 18-22. BNL ICP-MS had the best precision among all of the measurements. LANL TIMS, and even more so for PNNL ICP-MS, had poorer precision (by factors of about 1.5 and 4, respectively). It is likely that superb analytical blank control by BNL played a key role in their excellent performance for measurement precision. Although both LANL and PNNL ran internal blank controls, their results for the unspiked samples indicated additional sources of contamination.

BNL FTA's precision was 2-3 times poorer than for ICP-MS. This is because there are inherent precision limitations for FTA: a) when there are few tracks, track resolution is good, but there is poor statistics, and b) when there are many tracks, track resolution is poor, and precision and bias are adversely affected. These drawbacks, in part, account for the increasing uncertainty as plutonium concentration increased.

It is unclear at this time why the LANL TIMS and PNNL ICP-MS relative measurement precision increased as the plutonium concentration increased. In general, the reverse is expected because of higher ion fluxes. This point is left for future investigations.

### <u>Bias</u>

Figures 23-27 displays the percent bias at each <sup>239</sup>Pu concentration level. Interpretation of these results are complicated by measurements with poor precision. However, the clear message is that BNL ICP-MS has the best set of bias values. BNL ICP-MS results make an unambiguous statement of its terrific measurement capabilities for <sup>239</sup>Pu at the μBq level with its excellent accuracy and measurement precision. The excellent agreement with the NIST values lends support to the presumption that the test samples were stable and accessible during this exercise. The BNL ICP-MS value for the blank samples was extremely low, and was probably responsible for the good performance. It is noted, however, that there is a systematic negative bias. It will have to be left to future investigations to determine if the negative bias is due to a systematic difference in the certification of the <sup>242</sup>Pu tracer.

LANL TIMS had serious bias problems at the 18.5 and 46.3 nBq/g levels. However, excellent bias values were obtained at the 148 and 278 nBq/g levels, although with poorer precision. None-the-less, these results illustrate the potential for TIMS to improve and be competitive with ICP-MS. To improve its performance, LANL should begin addressing the unaccounted blank contamination.

PNNL ICP-MS bias steadily worsened as concentration levels dropped. These results are probably strongly linked to the extremely high value they observed from the blank samples. There is no technical reason to prevent PNNL from achieving the same

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performance capabilities as BNL ICP-MS.

The BNL FTA bias is larger than those from ICP-MS, but are somewhat better than LANL at the lower concentrations and poorer at higher concentrations. As mentioned before, the poorer FTA performance is related to track density. It would be possible for BNL FTA to improve its bias performance when internal tracers (chemical yield monitors) are used. The results of this study indicates that FTA can make measurements within about 80 percent of a true value, 99.7 percent of the time, over the <sup>239</sup>Pu 3.7-55.6 µBq range.

### **ANSI Performance Criteria**

All four laboratories demonstrated their ability to make traceable measurements, per ANSI N42.22 criteria, at the 148.4 and 277.7 nBq/g concentration levels. At the 18.5 and 46.3 nBq/g concentration level, however, only BNL's ICP-MS and FTA measurements were traceable. The FTA success at making traceable measurements at the lower concentration levels, however, was primarily due to relatively large total propagated uncertainties.

All four laboratories passed both the precision and bias ANSI N13.30 criteria at the 277.7 nBq/g level. Only BNL's ICP-MS passed the ANSI N13.30 criteria for all four concentration levels.

### Minimum Detectable Amount (MDA)

The estimated MDAs were derived from the ANSI N13.30 equations; the simplified equation,  $MDL = 4.65s_b + 3$ , was not used because of significant contributions from systematic biases.

The general MDA equation from ANSI N13.30, when  $\alpha$  and  $\beta$  are equal, is:

$$MDA = \frac{(1 \% \Delta_{\kappa}) (2\Delta_{B}B \% 2ks_{o} \% 3)}{\kappa T}$$
 (Eq 6)

where:

B = the total count of the appropriate blank,

 $s_0$  = the standard deviation in the net sample count of a subject with no additional analyte, defined by ANSI N13.30 Equation 2,

K = calibration factor, (including correction for self absorption when appropriate),

 $\Delta_{\rm K}$  = the maximum fractional systematic error bound in the calibration factor K, (like  $\Delta_{\rm B}$ ,  $\Delta_{\rm K}$  cannot be estimated using replicate measurements, and must be estimated by the professional judgment of the analyst),

 $\Delta_{\rm B}$  = the maximum expected fractional systematic error bound in the

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appropriate blank, (The factor of 2 before the  $\Delta_B$  takes into account the maximum systematic error bound when the background and sample measurement errors are of opposite sign),

k = the abscissa of the standardized normal distribution corresponding to the 0.05 probability level, for  $\alpha$  = 0.05 and  $\beta$  = 0.05, k = 1.645,

T = standard subject counting time for the procedure.

The MDA can be obtained from data in units of count-rate from:

$$MDA = (1 + \Delta_{K}^{\prime})(2\Delta_{B}B^{\prime} + 2ks_{0}^{\prime} + 3)/K^{\prime}$$
 (Eq 7)

where:

B' = B/T  $s_0' = s_0/T$ K' = K/T

 $\Delta_{\mathbf{k}} = \Delta_{\mathbf{k}}$  since they represent the same fractional systematic relative fixed error.

The unprimed quantities are used when total counts are used in the computation, and the primed quantities are used when the count rates are computed.

For this exercise, equation 7 was used to calculate MDAs. It was further assumed that  $\Delta_{k'} = \Delta_{B}$ . Because several blank sample results were not reported, and estimated uncertainties for the blank sample results were large, an extrapolation method was chosen to improve the reliability of estimating MDA's. MDA's were calculated on Spreadsheet 5 at each concentration level, and extrapolated back to "0" nBq/g (see Figures 30-33). BNL ICP-MS MDA's were fairly reproducible across the entire concentration range, the reported MDA for this study is the mean value, and the CI is reported as two standard deviations of the calculated MDA's. The estimated MDA's for the 200 g sample are as follows:

Laboratory	MDA (nBq/200g sample)	95% Confidence Interval (Percent)
BNL ICP-MS	1600	35
BNL FTA	1200	1900
LANL	009	290
PNNL	91000	3600

spectroscopy for 239Np in synthetic urine. FTA's MDA is comparable to that expected from mass spectroscopy, but is a (BNL ICP-MS and LANL TIMS) MDA is about 3000 times lower than for alpha spectroscopy. This is in contrast to the n general, routine alpha spectroscopy's MDA is about 3 x 10<sup>6</sup> nBq. These results indicate that mass spectroscopy's Thein, Health Physics, 68 (3), 350-358, 1995; An Intercomparison Study of Neptunium-237 Determination in study by Lee et al (Bioassay Procedures for Neptunium-237, S.C. Lee, J.M.R. Hutchinson, K.G.W. Inn, and M. Artificial Urine Samples, J.M. Robin Hutchinson, Shan Lee, and Kenneth G.W. Inn, Report to DoE DE-AIO5-910P21969, May 1993) where they found ICP-MS only had comparable measurement capabilities to alpha factor of 10-100 times less certain.

larger than LANL's, it is known with much better precision and confidence. The estimated BNL FTA and PNNL ICP-MS The best MDA's were obtained by BNL's ICP-MS and LANL's TIMS. Although the estimated BNL MDA is somewhat MDAs were determined with only poor precision.

### Summary

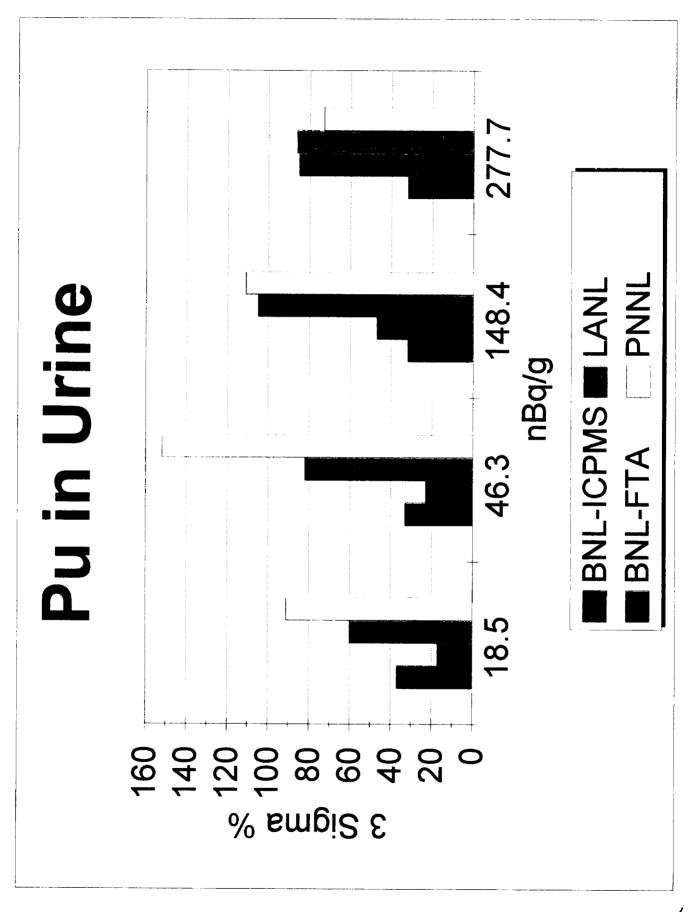
summarized in Spreadsheet 6. It is apparent that mass spectrometry is currently capable of successfully competing with FTA's sensitivity, and at considerably higher precision down to the 3.7 µBq/sample level. In addition, mass spectrometry has the potential to improve with new technology (e.g., new nebulizer design, multi-pulse detection systems, selective aser ionization) to provide more accurate and precise measurements than FTA. Chemical technologies can be improved with robotics, and the savings in terms of human resources can be shared by all three measurement The results of this study revealed the current potential of the ICP-MS, TIMS, and FTA capabilities. These are

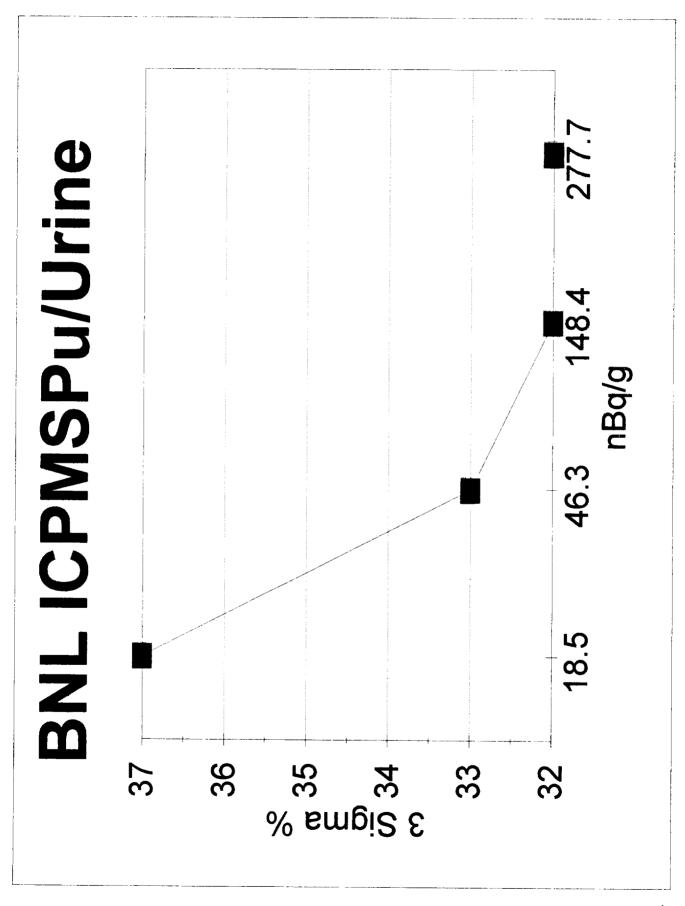
technologies. However, mass spectroscopy can eventually become more cost effective than FTA because of quicker turnaround times. ICP-MS, has apparently closed the precision gap with TIMS, and is very competitive with regards to accuracy and precision.

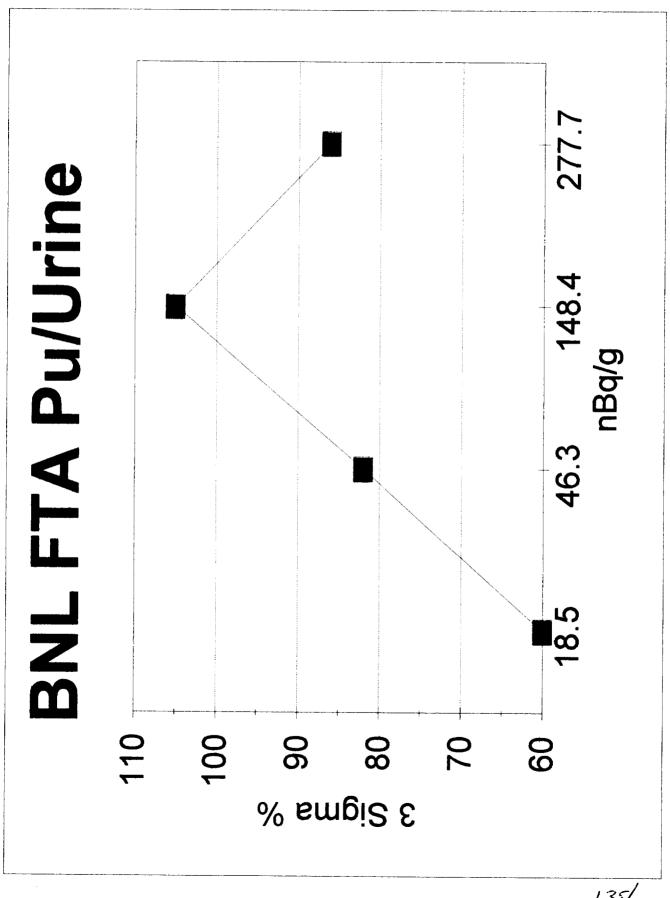
### In summary:

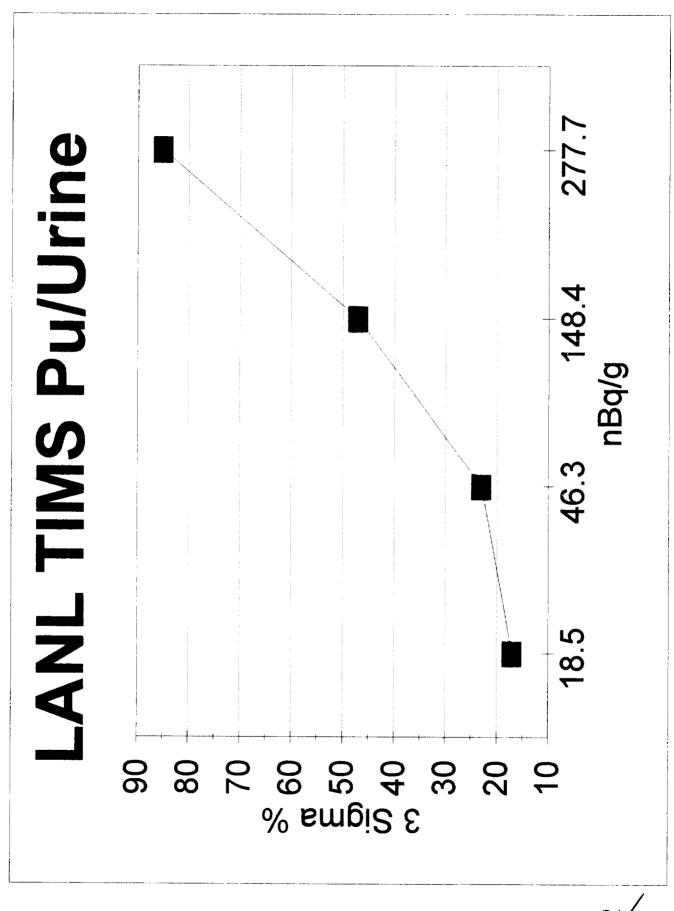
- o ICP-MS results indicated the tremendous potential to accurately and precisely measure µBq quantities of <sup>239</sup>Pu in synthetic urine, while maintaining competitive sensitivity (MDA) with FTA.
- o FTA can also measure μBq quantities of <sup>239</sup>Pu in synthetic urine, but with considerably larger uncertainty than mass spectroscopy.
- o TIMS also has the potential to also overtake FTA's measurement capabilities, but must make a considerable effort to identify and control root causes of high blanks and imprecision.
- O Controlling analytical blank is crucial for measuring ultra-low levels of <sup>239</sup>Pu in urine, which also means careful and exhaustive chemical separations cannot be avoided.
- The chemists must find ways to improve chemical yields to improve measurement sensitivity and reliability.

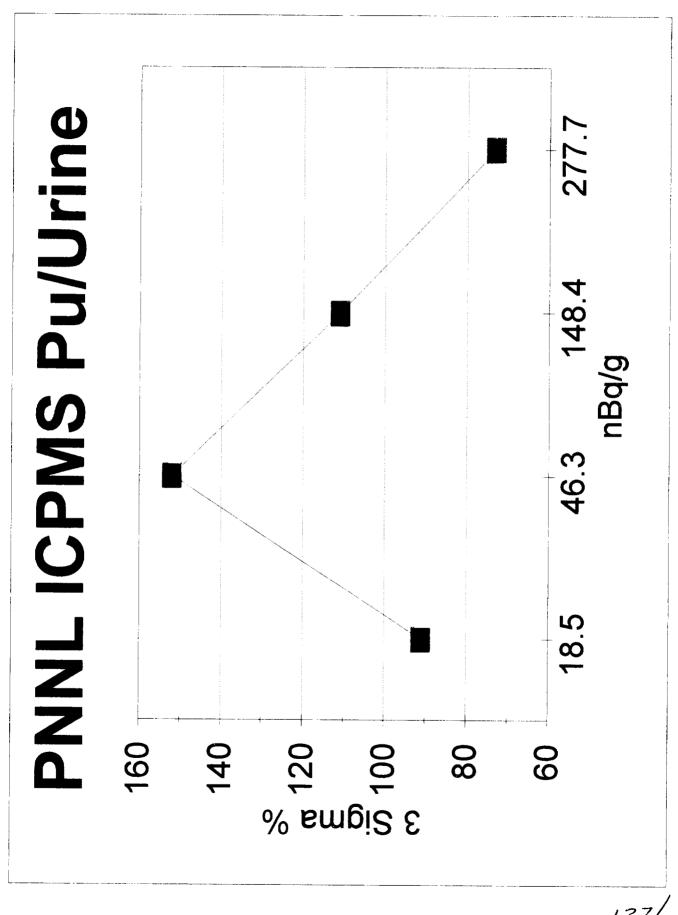
### Figures 18-22 Total Propagated Uncertainties



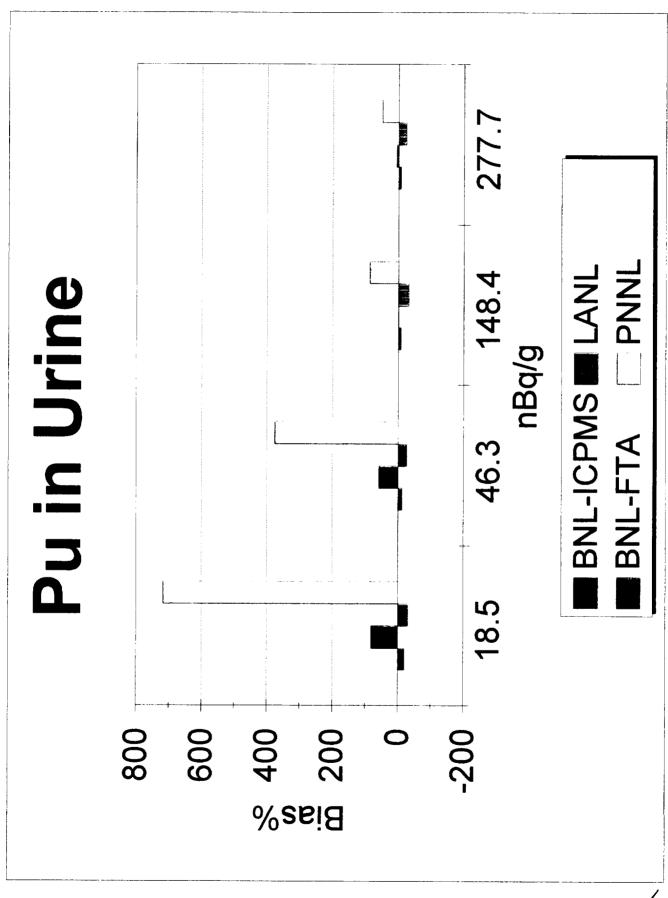


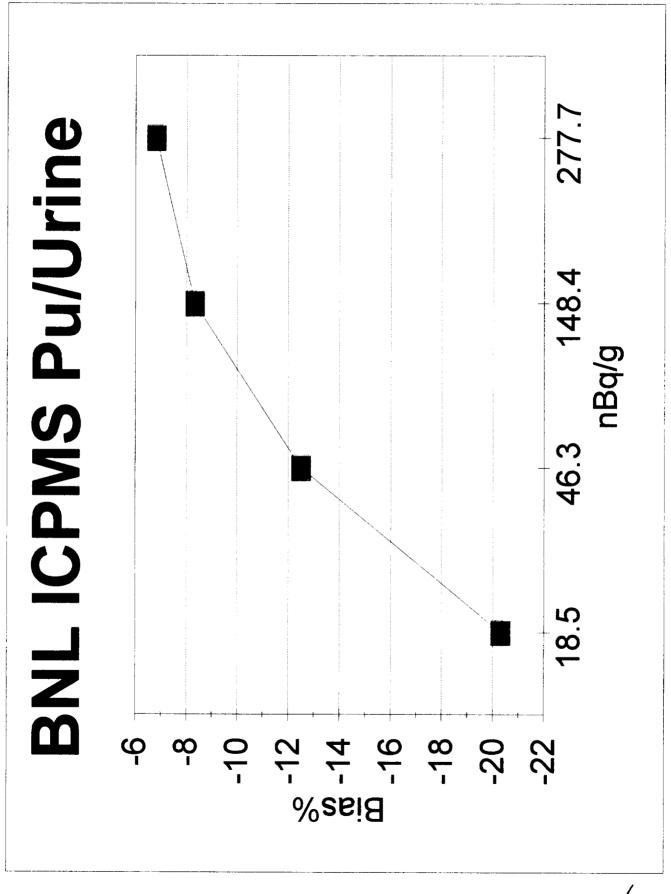


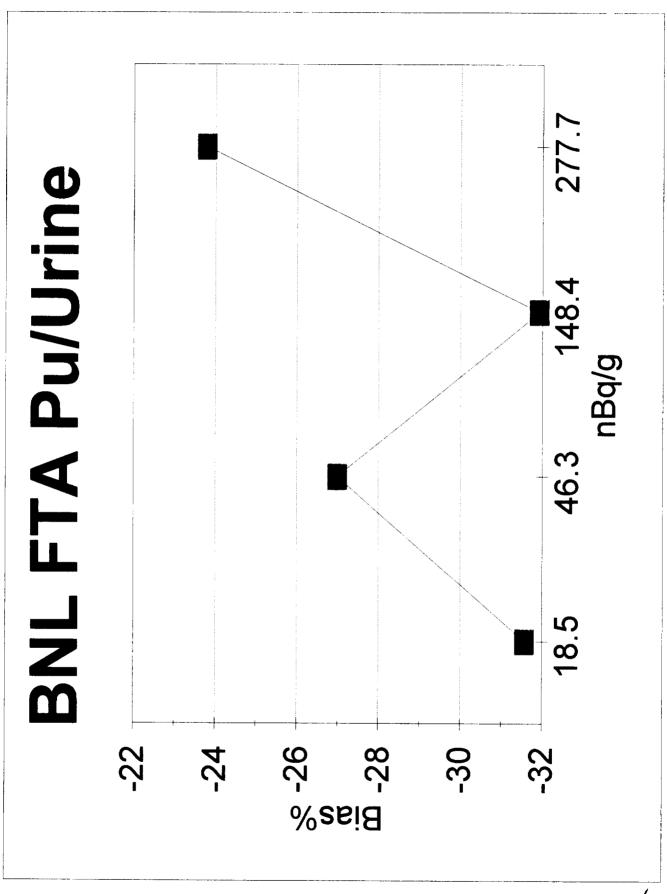


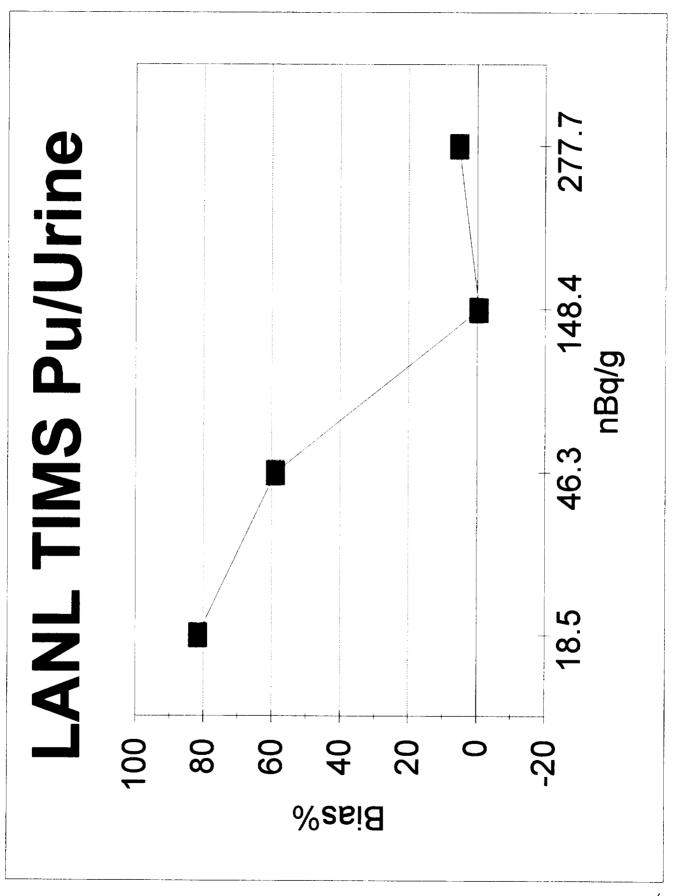


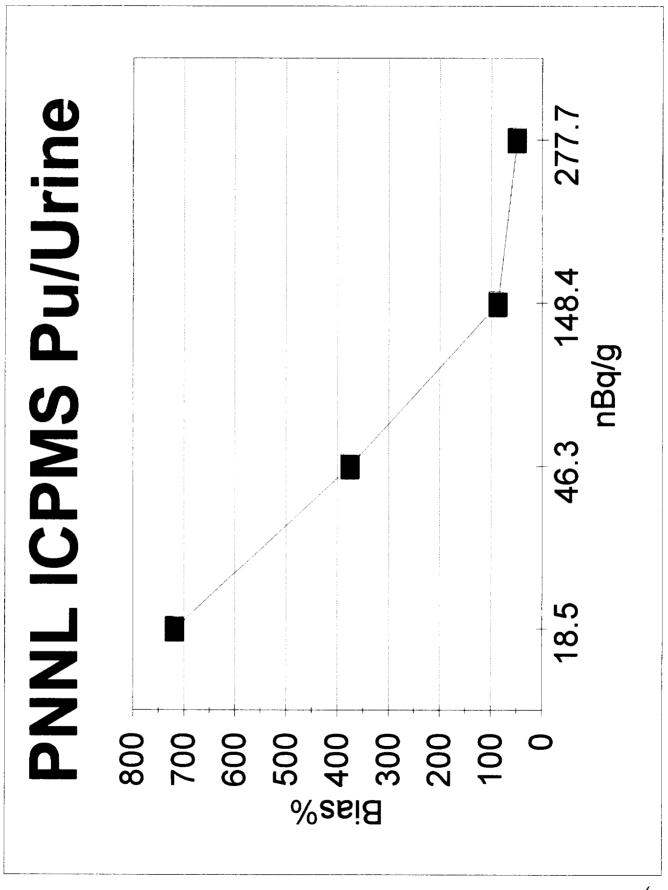
Figures 23-27
Bias











#### Spreadsheet 5 Minimum Detectable Amount

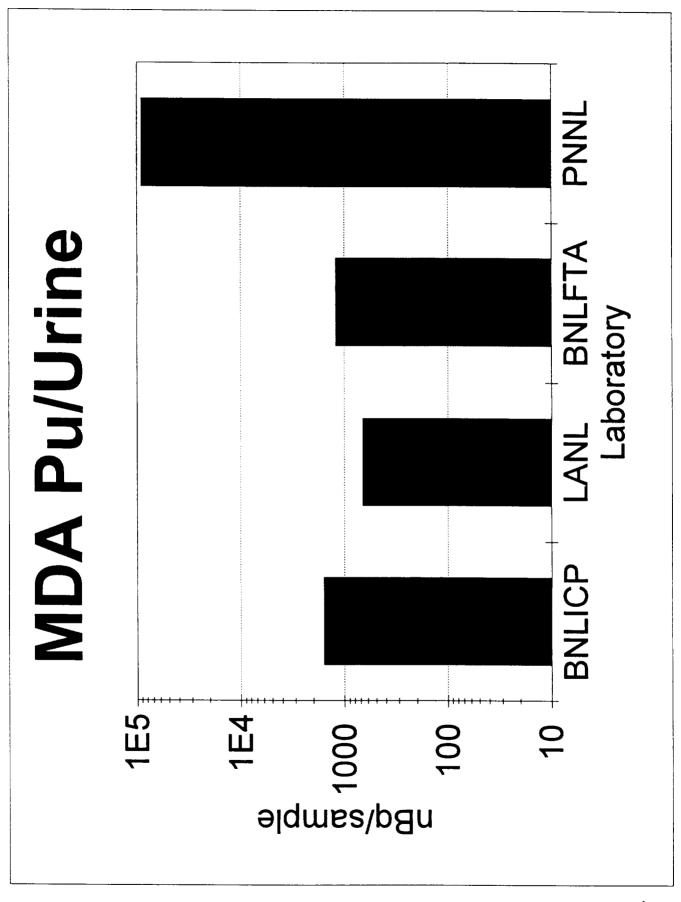
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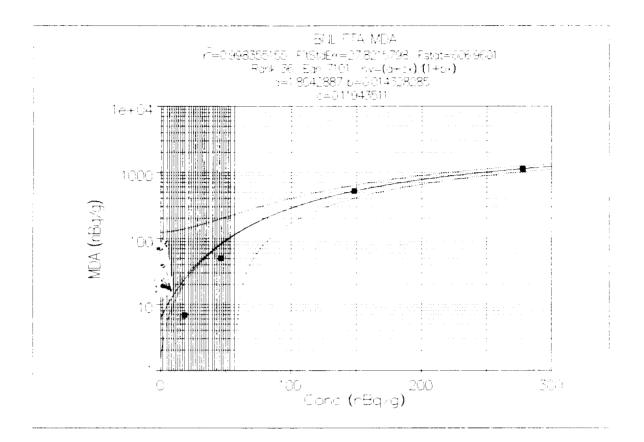
144

				_		7.9	22%					9	1900%					က	35%					455	3600%			
_			mda	at "0" nBq/g			CL95% =						CL95% = 19						CL95% = 585%						3E = %5670			
I			mda	nBq/g		9.242649	6.993474	7.40138	6.452636	9.593352		21.13697	6.826113	50.13683	517.8243	1122.893		131,1281	9.160743	21.48596	81.55305	315.1431		816.347	649.2829	5889.889	3982.039	
g			Systemmatic	sm1(nBq/g) sigma1(nBq/g nBq/g		0.002675	1.5836	4.3335	14.552	27.713		1.0395	2.4003	6.3882	19.089	40.068		0.131159	0.096432	0.210945	0.42189	0.83804		30.24	33.824	49.28	61.824	
u_			Random	sm1(nBq/g)		1.4828875	0.9496932	1.0488087	0.8164964	1.5632567		3.2659864	0.7657725	6.7186322	29.753156	45.742244		36.505576	1.8585712	5.5464702	22.891149	82.676588		35.000006	30.836797	100.0001	81.584303	
W			Systemmatic Random	sigma1%		10.7	10.7	10.7	10.7	10.7		18.9	18.9	18.9	18.9	18.9		0.287	0.287	0.287	0.287	0.287		22.4	22.4	22.4	22.4	
۵			Random	sm1%		5931.55	6.416846	2.589651	136 0.600365	259 0.603574		59.38157	6.029705	19.87761	29.45857	21.57653		79.88091	5.531462	7.546218	15.57221	28.3139		25.92593	20.42172	45.45455	29.55953	
ပ			Reported	nBq/g		-0.025	14.8	40.5	136	259		5.5	12.7	33.8	101	212		45.7	33.6	73.5	147	292		135	151	220	276	
8			NIST	nBq/g		BLANK	18.5	46.3	148.4	277.7		BLANK	18.5	46.3	148.4	277.7		BLANK	18.5	46.3	148.4	277.7		BLANK	18.5	46.3	148.4	
4	mda		lab			BNL ICP-MS						BNL FTA						LANL TIMS						PNNL ICP-M				
-	-	7	ဗ	4	တ	9	7	80	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	

## Figures 28-31 Minimum Detectable Amount

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BNL FTA MDA Sep 9,1997 11:26 PM

5 Active X-Y Points

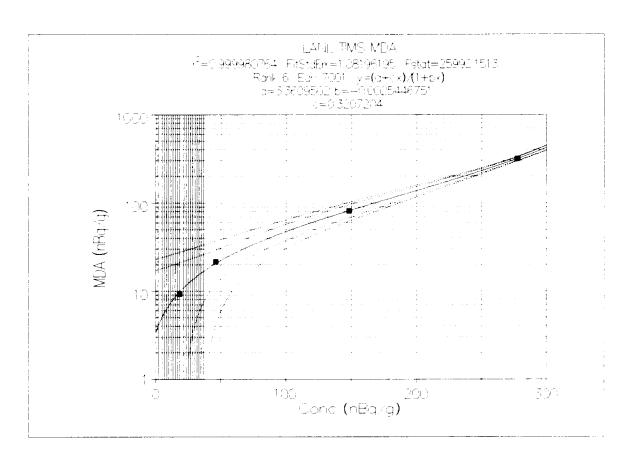
X: Conc (nBq/g) Mean: 98.18 SD: 115.57381624 Y: MDA (nBq/g) Mean: 343.7634426 SD: 485.06990265

File Source:

Rank 36 Eqn 7101 lny=(a+cx)/(1+bx)

r2 Coef Det DF Adj r2 Fit Std Err F-value 0.9983551552 0.9934206209 27.821579826 606.96010035

Parm Value Std Error t-value 95% Confidence Limits а 1.804288718 1.121621043 1.608643783 -2.84635413 6.454931566 0.00460172 -0.0047521 b 0.014328285 3.113680267 0.033408666 0.119435114 0.036337588 3.286820091 -0.03123355 0.270103778 С



LANL TIMS MDA Sep 9,1997 11:33 PM

4 Active X-Y Points

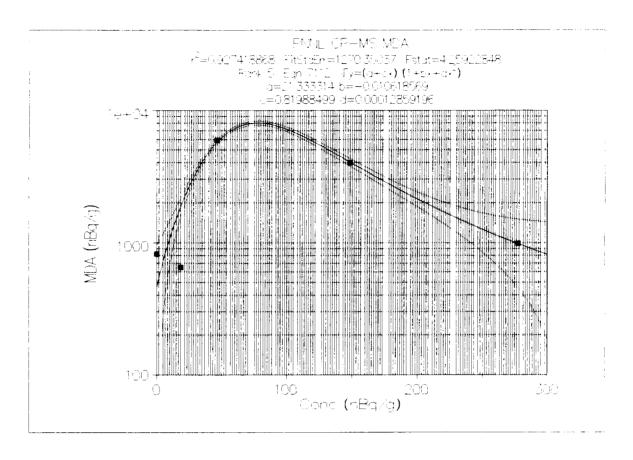
X: Conc (nBq/g) Mean: 122.725 SD: 117.44514677 Y: MDA (nBq/g) Mean: 106.83571325 SD: 142.42677724

File Source:

Rank 6 Eqn 7001 y=(a+cx)/(1+bx)

r2 Coef Det DF Adj r2 Fit Std Err F-value 0.9999807638 0.9999422914 1.0819619474 25992.151267

Parm Value Std Error t-value 95% Confidence Limits 3.360950177 1.068903689 3.144296544 -10.4214387 17.14333908 a -0.00254468 4.15384e-05 -61.260773 -0.00308027 -0.00200908 b 0.320720403 0.014819793 21.64135539 0.129634761 0.511806046



PNNL ICP-MS MDA Sep 9,1997 11:47 PM

5 Active X-Y Points

X: Conc (nBq/g) Mean: 98.18 SD: 115.57381624 Y: MDA (nBq/g) Mean: 2464.66464 SD: 2357.6626151

File Source:

Rank 5 Eqn 7112 SQRTy=(a+cx)/(1+bx+dx2)

r2 Coef Det DF Adj r2 Fit Std Err F-value 0.9274188685 0.7096754739 1270.3503745 4.2592284846

Parm Value Std Error t-value 95% Confidence Limits 21.3333141 39.26795737 0.543275371 -484.985698 527.6523259 а b -0.01061857 0.007909886 -1.34244268 -0.11260824 0.091371098 1.062183822 0.771886157 -12.8758583 14.51562827 С 0.819884989 0.000128592 0.000114773 1.120405329 -0.00135128 0.001608465

## VIII. CONCLUSIONS

The prime objective of this study was to assess the current capabilities of FTA, ICP-MS and TIMS to measure µBq quantities of <sup>239</sup>Pu in urine. It is clear that all three methods have the capabilities to make such measurements. BNL's excellent ICP-MS work demonstrated that accurate and precise measurements are already a reality. This reality, however, is probably dependent on the laboratory's ability to minimize and control the analytical blank. Such control can only be achieved with highly skilled professionals, in dedicated ultra-clean laboratory facilities, with ultra-pure reagents. These requirements will be costly, but necessary. Measurements of such small quantities of plutonium is technically difficult, and lost data (21% in this study) or repeat analysis must be minimized with robust analytical and measurement procedures. Although FTA does not have the analytical precision of high quality ICP-MS, this study has demonstrated that it potentially has comparable MDA to ICP-MS. Unless the inherent disadvantages of FTA (batch yield correction, track overlap, and poor statistics) can be overcome, it is advantageous that a larger share of development resources be focused on mass spectrometric analyses. While TIMS did not provide the high accuracy and precision of BNL ICP-MS, it is likely that it too could be improved to be competitive and deserves development. Both ICP-MS and TIMS could enhance their capabilities considerably through minimization and control over analytical blank, higher chemical recovery, improved precision, and higher accuracy yield monitors. With future improvements in technology and techniques, it is anticipated that ICP-MS and TIMS will satisfactorily meet the ANSI N42.22 criteria for traceability and the ANSI N13.30 criteria for bias and precision, even at these amazingly low concentrations of plutonium in the complex urine matrix.

Secondarily, the technical issues of test sample preparation and stability have been addressed. This study has demonstrated that careful serial dilutions of the plutonium SRM over nine orders of magnitude to nBq/g concentrations can be done accurately, that the dilutions can be confirmed by measurement within a few percent, and the plutonium in synthetic urine remains stable and accessible for analysis (to within 5 percent) for at least a few weeks. The success of this study confirms the efficacy of the protocol to prepare these test materials.

### IX. RECOMMENDATIONS

It is recommended that improvements to the accuracy, precision and sensitivity of plutonium-in-urine Mass Spectrometry metrology for reliable DOE/EH occupational worker's health and safety, validating excretion models; identification of the source-terms; and litigation dispute resolution be initiated by:

- Evaluating and contrasting techniques, during on-site assessments, of BNL, LANL and PNNL to determine the critical elements for success by the BNL ICP-MS:
  - o Evaluate sources of laboratory blank contamination,
  - o Evaluate why the Labs had difficulty with the Blanks,
  - o Evaluate why the Labs had low chemical yields,
  - o Evaluate why the Labs had large measurement imprecision,
  - o Evaluate why the Labs had analytical bias.
- 2. Developing a consistent method to calculate FTA and ICP-MS measurement uncertainties and detection limits.
- 3. Preparing Standard Reference Material <sup>242</sup>Pu at chemical yield tracer at 11.1 µBq/g level for use by the mass spectroscopy community.
- 4. Conducting intercomparison of <sup>239</sup>Pu in the range of 1500-100 aCi/200 mL of synthetic urine containing chemical and isobaric interferences: <sup>240</sup>Pu, <sup>241</sup>Pu, and trace-elements too more carefully test ICP-MS, TIMS and FTA under more realistic conditions.

# X. ACKNOWLEDGMENTS

The author gratefully acknowledges the expertise provided by David McCurdy and Leenu Kuruvella (YAEL), and the measurement expertise of Edward Kaplan (BNL), Peggy Gautier and Moses Attrep (LANL), and Eric Weiss (PNNL). The author also acknowledges the constant support by Neil M. Barss and R. Thomas Bell III (DOE-EH63) through contract number DE-Al01-96EH96203.

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